Gibson Hill Road and Crocker Lane

Intersection Alternatives Analysis Memorandum

Prepared for:

City of Albany, Oregon



Prepared By:

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February 2016

Alternatives Analysis Memorandum



Introduction

The Gibson Hill Road and Crocker Lane intersection is a three-leg "T" intersection with stop-control on the Crocker Lane approach. The intersection is located in North Albany, and connects residential areas to the north to an east-west connection between rural lands and an urban center. Crittenden Loop intersects Gibson Hill Road 160 ft to the east of the intersection with Crocker Lane. As development continues in the area, traffic volumes at the intersection with Crocker Lane are anticipated to grow leaving residents concerned with increasing delays and worsening conditions for bike and pedestrian crossings of Gibson Hill Road. These concerns have prompted the City of Albany to consider traffic control improvement alternatives at this intersection. The City of Albany and Benton County Transportation System Plans both recommend the improvement of Gibson Hill Road to an urban minor arterial with improved traffic control at the intersection with Crocker Lane.

Purpose

The purpose of this memorandum is to provide the City of Albany and Benton County with a summary evaluation of the performance, cost, safety considerations, and impacts of each intersection concept design alternative.

Existing Conditions

The existing intersection is controlled by a stop sign on the southbound approach of Crocker Lane. The speed on Gibson Hill Road is 40 mph to the east and 45 mph to the west. Crocker Lane is posted at 35 mph. Bike and pedestrian crossings of Gibson Hill Road are currently accommodated by a Rectangular Rapid Flash Beacon (RRFB) and striped crosswalk.



City of Albany Minimum Performance Standards

The City of Albany defines the minimum performance standards for intersections with different traffic control in their *Traffic Impact Study Guidelines*.

Traffic Control	Minimum Performance Standard
Traffic Signal and All-Way Stop	Level of Service (LOS): D
Uncontrolled and Two-Way Stop (worst case movement)	Volume-to-Capacity (V/C): 0.85

Crash Analysis

Five years of the most recent crash data available (January 1, 2010 to December 31, 2014) was obtained from the Oregon Department of Transportation for a review of existing crash history. In total there were four crashes recorded at the intersection between Gibson Hill Road and Crocker Lane and 3 crashes recorded on the approaches of Gibson Hill Road within 250 ft of the intersection. Of the crashes at the intersection, all four were turning movement crashes involving a vehicle making a left turn from Crocker Lane. One of these crashes involved a bicycle and resulted in serious injuries. The crashes on the Gibson Hill Road

approaches included one rear-end crash, one crash involving an animal, and one turning movement crash involving a vehicle turning from the nearby intersection with Crittenden Loop. The crash rate observed at this intersection is below the 90th percentile statewide crash rates for a 3-way stop-controlled intersection, produced by the Oregon Department of Transportation. This indicates that the crash rate at this intersection is within a typical range for similar intersections around the state.

All-Way Stop Warrants

Conditions for installing an all-way stop controlled intersection are established by the 2009 Manual of Uniform Traffic Control Devices (MUTCD). The criteria for all-way stop control include an analysis of eight-hour intersection volumes, crash history, delay, and speed. All-way stop control can also be used as an interim measure at locations found to justify traffic signal control. Current traffic volumes at the intersection of Gibson Hill Road and Crocker Lane currently satisfy the requirements for installation of all-way stop control.

Signal Warrants

There are eight signal warrants established by the MUTCD that are used to evaluate the need for a traffic signal at a given intersection. Three of these warrants are based solely on traffic volumes: Warrant 1 – 8-hour Traffic Volumes, Warrant 2 – 4-hour Traffic Volumes, and Warrant 3 – Peak Hour Traffic Volumes.

After comparing existing (2016) turning movement volumes on the Gibson Hill Road and Crocker Lane intersection it was determined that two of the volume-based warrants are currently met by 2016 volumes. The 4-hour traffic volume warrant and peak hour warrant are satisfied based on 2016 volumes because based on city provided data the 85th percentile speeds on Gibson Hill Road are in excess of 40 mph. Volume thresholds for traffic signal warrants increase where typical travel speeds do not exceed 40 mph; therefore, if travel speeds on Gibson Hill Road did not exceed 40 mph the current 2016 traffic volumes would not meet volume warrants. Traffic signal warrant spreadsheets are attached to this report.

Summary of Existing Performance

The existing intersection configuration, a stop-controlled southbound approach (Crocker Lane), currently meets operational standards with a volume-to-capacity ratio of 0.44 for the southbound approach during the afternoon peak hour. During peak conditions, vehicles stopped on Crocker Lane may experience delays while waiting for appropriate gaps to turn onto Gibson Hill Road. As volumes on Gibson Hill Road continue to increase with development, delays on Crocker Lane are expected to increase. Bicycle and pedestrian crossings of Gibson Hill Road are currently accommodated with a Rectangular Rapid Flash Beacon (RRFB).

Alternatives Analysis Methodology

Each proposed alternative was evaluated to understand the impacts, performance and costs of the proposed intersection configurations. Concept-level designs were created to estimate the potential right-of-way impacts, constraints, and planning-level cost opinions (does not include costs of ROW, utility relocations, hazmat, environmental mitigation, etc.). Traffic analysis was completed to identify the expected operations of each configuration based on projected future year (2040) traffic volumes provided by the City of Albany. Year 2040 volumes are intended to closely approximate buildout of the current UGB boundary in North Albany. Qualitative evaluation of geometric safety considerations, bike and pedestrian facilities, and fatal flaws is also presented. Specific findings for each alternative are presented below by alternative. The findings of this evaluation are summarized within this report by Alternative. A summary of findings is presented in a matrix at the end of this heading.

Alternative 1:

All-Way Stop Control





Conceptual Design

- ✓ Re-stripe the intersection to include stop-bars and stop-signs at each roadway approach.
- ✓ Remove the existing Rectangular Rapid Flash Beacon (RRFB).
- More detailed design information is included in the concept design sheet attached to this memorandum.

Right-Of-Way Impacts

The all-way stop control intersection alternative requires no additional right-of-way.

2040 Traffic Operations

In 2040, the all-way stop controlled intersection does not meet operational standards during the afternoon peak hour with a volume-to-capacity ratio of 1.10 for the westbound approach. It is likely that operations would only fail to meet minimum standards during the peak hour and would operate sufficiently for the rest of the day. Queuing results obtained from a Highway Capacity Manual (HCM) analysis don't indicate significant queuing with this alternative; however, the queuing for this alternative is expected to be similar to what would be experienced for the roundabout alternatives since the HCM analysis typically underestimates queuing for all-way stop-controlled intersections.

Geometric Safety Evaluation

Installation of all-way stop-control may reduce the frequency of turning movement and angle collisions at the intersection. There is potential for short-term increases in specific crash types, such as rear-end crashes, while drivers become accustomed to the change in traffic control to an all-way stop. Sight distance evaluation should be completed to ensure final intersection configuration meets standards.

Bike and Pedestrian Considerations

Bikes would continue to use the striped bike lane/shoulders. The striped crosswalk at all-way stop intersections provide some level of protection; however, the stop-signs at the all-way stop control may not provide the same level of driver warning as the existing RRFB.

Cost Estimate

Construction: \$6,000 Contingency: \$1,500 Preliminary Engineering: \$2,000 TOTAL: \$9,500

2040 Traffic Operations

- Meets standards in the AM peak hour
- Does not meet standards in the PM peak hour

Worst Queuing:

Queuing is expected to be similar to what is experienced with the roundabout alternatives in the AM and PM peak hours

Future Considerations

 Potential as an interim, low-cost alternative until ultimate corridor design configuration is decided (roundabouts vs. signals, etc.)

Alternative 2:

Single Lane Traffic Signal



Conceptual Design

- ✓ Install a traffic signal and maintain single lane approaches.
- ✓ New ADA pedestrian ramps on the northeast and northwest corners of the intersection.
- ✓ Striped crosswalks on the north and east legs of the intersection.
- ✓ Pavement widening to accommodate the turning radius for a large semitrailer (WB-50 design vehicle).
- ✓ Remove the existing RRFB.
- Existing bus pullout on the south side of Gibson Hill Road remains.
- More detailed design information is included in the concept design sheet attached to this memorandum.

Right-Of-Way Impacts

The right-of-way impacts for a single lane traffic signal are minimal. The only right-of-way impacts are at the northwest and northeast corners of the intersection (illustrated by red hatching above) for the ADA pedestrian ramps.

2040 Traffic Operations

In 2040, the single lane traffic signal operates under adopted standards with a LOS B in the morning and afternoon peak periods. Queuing in the westbound direction is expected to back up well past the intersection with Crittenden Loop. Access restriction on Gibson Hill Road should be considered at this location.

Geometric Safety Evaluation

Traffic signals are generally recognized as reducing the frequency of specific crash types, primarily angle and turning movement crashes. However, the introduction of traffic signals can also increase the frequency of other types of crashes, most notably rear-ends.

Bike and Pedestrian Considerations

Bikes will continue to use striped bike lane/shoulders. Pedestrians will benefit from striped crosswalks and pedestrian push buttons for controlled pedestrian crossings. Maintaining single lane approaches means that the pedestrian crossing distance is shorter than at a traffic signal with turn lanes.

Cost Estimate

Construction: \$311,000 Contingency: \$156,000 Preliminary Engineering: \$71,000 TOTAL: \$538,000

2040 Traffic Operations

Meets standards in the AM and PM peak hours

Worst Queuing:

Eastbound: 225 ft (AM) Westbound: 350 ft (PM) Southbound: 200 ft (AM)

Future Considerations

- Consider future plans for Gibson Hill Rd corridor (roundabouts vs. signals)
- May require access control on Gibson Hill Road at Crittenden Loop
- Potential for increased delay to side-street volumes in off-peak hours

Alternative 3:

Traffic Signal with Turn Lanes





Conceptual Design

- ✓ Install a traffic signal with left-turn lanes in the eastbound and southbound directions and a right-turn lane in the westbound direction.
- ✓ Remove the existing RRFB and relocate existing overhead utilities.
- ✓ ADA pedestrian ramps with striped crosswalks.
- ✓ Reconfigure the existing bus pullout on the south side of Gibson Hill Road.
- ✓ Restrict access to Crittenden Loop as it's located within the taper for the westbound right-turn lane.
- ✓ Lane widths include: 11' travel lanes, 12' turn lanes, 5' bike lanes/shoulders, and right-of-way for 6 ft sidewalks.
- Designed to accommodate the turning radius of a large semitrailer (WB-50 design vehicle).
- ✓ More detailed design information is included in the concept design sheet attached to this memorandum.

Right-Of-Way Impacts

The right-of-way impacts for this alternative are localized to the north side of Gibson Hill Road (illustrated by red hatching above).

2040 Traffic Operations

In 2040, the signalized intersection with turn lanes operates under adopted standards with an overall LOS A during the morning and afternoon peak hours. While traffic signals may decrease side street delay during peak periods, it's possible that Crocker Lane may experience additional delay during off peak hours, where acceptable gaps in oncoming traffic are more frequent and signalization isn't needed. Turn lanes improve vehicular operations and reduce queuing when compared to Alternative 2.

Cost Estimate

Construction: \$1,084,000 Contingency: \$542,000 Preliminary Engineering: \$244,000 TOTAL: \$1,870,000

2040 Traffic Operations

Meets standards in the AM and PM peak hours

Worst Queuing:

Eastbound: 200 ft (AM) Westbound: 150 ft (PM) Southbound: 100 ft (AM)

Future Considerations

- Consider future plans for Gibson Hill Rd corridor (roundabouts vs. signals)
- Access control at Crittenden Loop
- Right-turn lane conflict with bike lanes
- Potential for increased delay to side-street volumes in off-peak hours

Geometric Safety Evaluation

Traffic signals are generally recognized as reducing the frequency of specific crash types, specifically angle and turning movement crashes. However, the introduction of traffic signals can also increase the frequency of other types of crashes, most notably rearends.

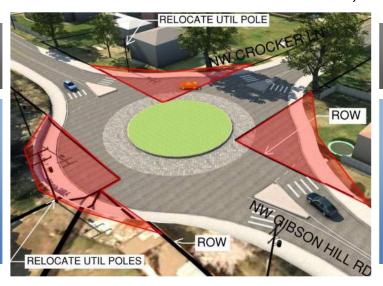
Bike and Pedestrian Considerations

Bikes will continue to use striped bike lane/shoulders. Pedestrians will benefit from crosswalks and pedestrian push buttons for controlled pedestrian crossings. Right-turn lanes result in increased pedestrian crossing distance/exposure and create potential conflicts with bicyclists along Gibson Hill Road.

Alternative 4:

Modern Roundabout





Conceptual Design

- ✓ Install a modern roundabout with an inscribed diameter of 115 ft, a 50 ft diameter raised island and 12 ft mountable truck apron.
- ✓ Existing bike lanes would be routed up on to 10' multi-use sidewalks around the perimeter of the roundabout.
- ✓ Designed to accommodate a large semitrailer (WB-50 design vehicle).
- ✓ Remove or relocated existing RRFB.
- Relocate existing utility poles.
- ✓ Relocate existing bus pullout on the south side of Gibson Hill Road.
- ✓ Restrict access on Gibson Hill Road to Crittenden Loop.
- ✓ A speed study should be completed to inform final design of traffic calming features for a full roundabout.
- ✓ More detailed design information is included in the concept design sheet attached to this memorandum.

Right-Of-Way Impacts

Additional right-of-way is needed on the north and south side of Gibson Hill Road in order to avoid property building takes at the north side of the intersection.

2040 Traffic Operations

In 2040, the modern roundabout operates under adopted standards with a LOS B in the morning and afternoon peaks. Queuing in the westbound direction is expected to extend back past the intersection with Crittenden Loop during the afternoon peak. Access control on Gibson Hill Road at this location may be required.

Geometric Safety Evaluation

Roundabouts reduce the number of crossing conflicts at an intersection which may result in a reduced frequency of severe turning movement conflicts. In general, traffic calming measures can be incorporated into the geometric design of roundabouts which may also help reduce excessive vehicular speeds along Gibson Hill Road.

Cost Estimate

Construction: \$848,000 Contingency: \$424,000 Preliminary Engineering: \$191,000 TOTAL: \$1,463,000

2040 Traffic Operations

Meets standards in the AM and PM peak hours

Worst Queuing:

Eastbound: 250 ft (AM) Westbound: 250 ft (PM) Southbound: 100 ft (AM)

Future Considerations

- Speed study to inform design of roundabout with potential, supplemental traffic calming measures to consider pedestrian safety
- Access control at Crittenden Loop
- Intersection re-alignment to avoid property building take
- Consider future plans for Gibson Hill Rd corridor (roundabouts vs. signals)

Bike and Pedestrian Considerations

A 10 ft multi-use sidewalk around the perimeter of the roundabout would accommodate bikes and pedestrians. Crosswalks at each approach should be separated by medians to facilitate two-stage pedestrian crossings. The existing RRFB can be relocated in combination with a roundabout.

Alternative 5:

Mini Roundabout





Conceptual Design

- ✓ Install a mini roundabout with an inscribed diameter of 60 ft and a 25 ft diameter mountable center island.
- ✓ Striped splitter island needed to accommodate a large semitrailer (WB-50 design vehicle).
- ✓ Remove or relocate the existing RRFB.
- ✓ Relocate existing utilities on the north and south sides of the intersection.
- ✓ Bikes to navigate through the roundabout with shared lanes.
- ✓ 6 ft sidewalks along the perimeter for pedestrians.
- ✓ Existing bus pullout is not affected; consider relocating with mini roundabout.
- More detailed design information is included in the concept design sheet attached to this memorandum.

Right-Of-Way Impacts

Right-of-way impacts for the mini roundabout are localized to the northwest and northeast corner of the intersection, as shown by the red hatching above.

2040 Traffic Operations

In 2040, the mini roundabout operates below adopted standards with a LOS C in the morning peak hour and LOS B in the afternoon peak hour. Queuing in the eastbound direction is expected to extend back approximately 350 ft during the morning peak hour while queuing in the westbound direction will back up past the intersection with Crittenden Loop during the afternoon peak hour. Access restrictions may be required at this location.

Geometric Safety Evaluation

According to the Federal Highway Administration's (FHWA) *Technical Summary on Mini Roundabouts*, mini roundabouts cannot provide the same level of speed reduction as a full roundabout and are less suited for roads with speeds exceeding 30 to 35 mph. Since speeds are currently in excess of 35 mph, a speed study would be required to evaluate the potential for reducing posted speeds through the corridor. If corridor improvements are implemented that result in lower speeds, it's possible that the safety benefits of a full roundabout such as decreased frequency of severe turning movement crashes and traffic calming may be realized.

Bike and Pedestrian Considerations

A 6 ft sidewalk around the perimeter of the roundabout would accommodate pedestrians with crosswalks and splitter islands at each approach to facilitate two-stage pedestrian crossings. Based on design guidance for mini roundabouts, bicyclists would share the travel lanes with vehicles through the mini roundabout. Speeds on Gibson Hill Road would need to be lowered to achieve recommended travel speeds in order to create a safe environment for bikes and pedestrians. The existing RRFB can be relocated in combination with a mini roundabout.

Cost Estimate

Construction: \$163,000 Contingency: \$82,000 Preliminary Engineering: \$37,000 TOTAL: \$282,000

2040 Traffic Operations

 Meets standards in the AM and PM peak hours

Worst Queuing:

Eastbound: 350 ft (AM) Westbound: 300 ft (PM) Southbound: 125 ft (AM)

Future Considerations

- Speed study to evaluate speed reductions on Gibson Hill Road
- Access control at Crittenden Loop
- Consider future plans for Gibson Hill Rd corridor (roundabouts vs. signals)

2040 Traffic Operations

If the existing intersection configuration is left in place until 2040 (future analysis year) the intersection can be expected to operate over minimum standards for two-way stop controlled intersections with a volume-to-capacity ratio greater than 0.85 for the southbound approach in the morning and afternoon peak period. Delays on Crocker Lane can be expected to increase as volumes through the intersection continue to grow.

Alternatives Analysis and Evaluation Summary

		Cost*	ROW Impacts	2040 Traffic		Safety	Bike/ Ped Facilities
STOP	Alternative 1: All-Way Stop Control	\$9,500	+	AM	PM -	✓	√
186	Alternative 2: Single Lane Traffic Signal	\$538,000	\checkmark	√	√	√	\checkmark
	Alternative 3: Traffic Signal with Turn Lanes	\$1,870,000	✓	+	+	√	-
5	Alternative 4: Modern Roundabout	\$1,463,000	-	+	+	+	√
	Alternative 5: Mini Roundabout	\$282,000	✓	+	+	+	-

^{*}Costs do not include ROW, utilities, hazmat or environmental mitigation

Summary and Conclusions

Current conditions at the intersection of Gibson Hill Road and Crocker lane meet operational standards; however, during peak conditions, delays for side street volumes will continue to increase as traffic volumes grow. While there is no immediate need for intersection improvements to meet operational standards, concerns regarding side-street delay and intersection safety warrant evaluation of potential alternatives for future intersection configurations. In general, each of the five intersection alternatives provide a feasible alternative for addressing current, and future, safety and operational concerns as they relate to the existing intersection configuration of Gibson Hill Road and Crocker Lane. The all-way stop controlled alternative is the only alternative that fails to meet operational standards in 2040; however, the implementation of an all-way stop controlled intersection could be a low-cost, interim solution to address current concerns while maintaining maximum flexibility for the ultimate configuration of the corridor. Signalization and roundabout alternatives provide varying benefits, as outlined within this report. The detailed technical information used to summarize performance within this memorandum can be found within the technical attachments included with this report.

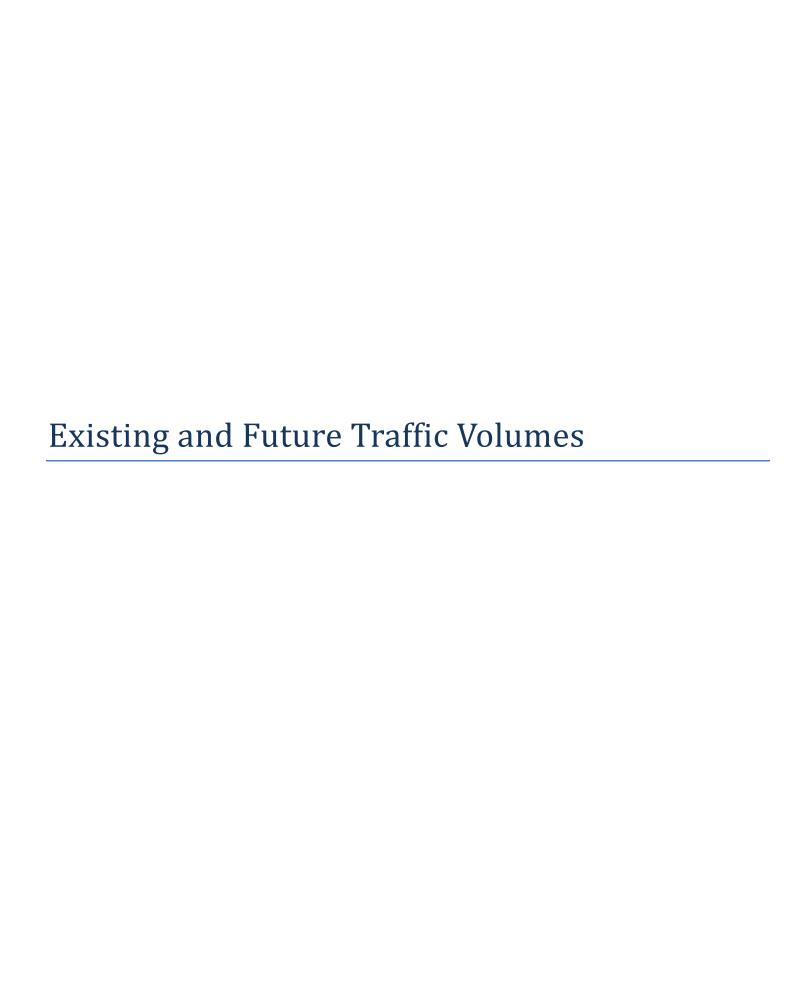
Acceptable Performance/
 Minimal Impact

⁺ Above Average Performance/ Little to no impact

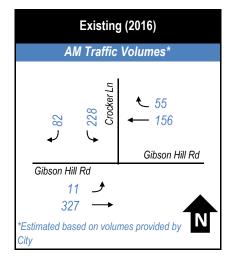
Below Average Performance/ Significant impact

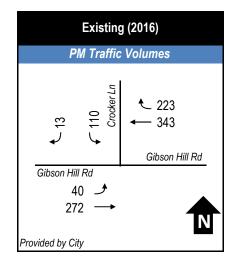
Technical Attachments

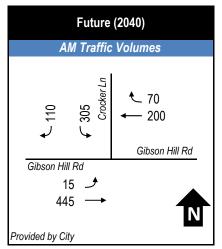
- Existing and Future Traffic Volumes
- Concept Design Sheets
- Preliminary Cost Estimates
- Traffic Operations Output
- Crash History

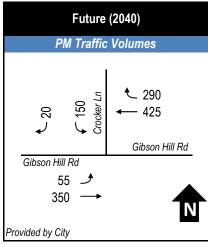


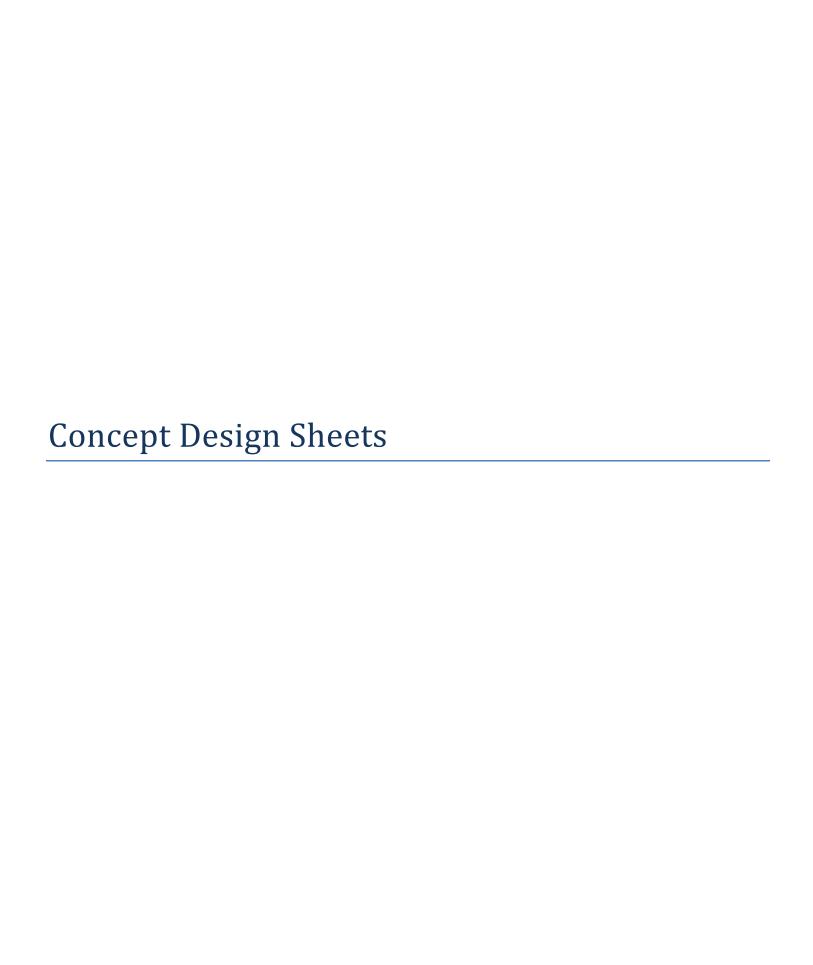
Traffic Volumes - Gibson Hill Road at Crocker Lane



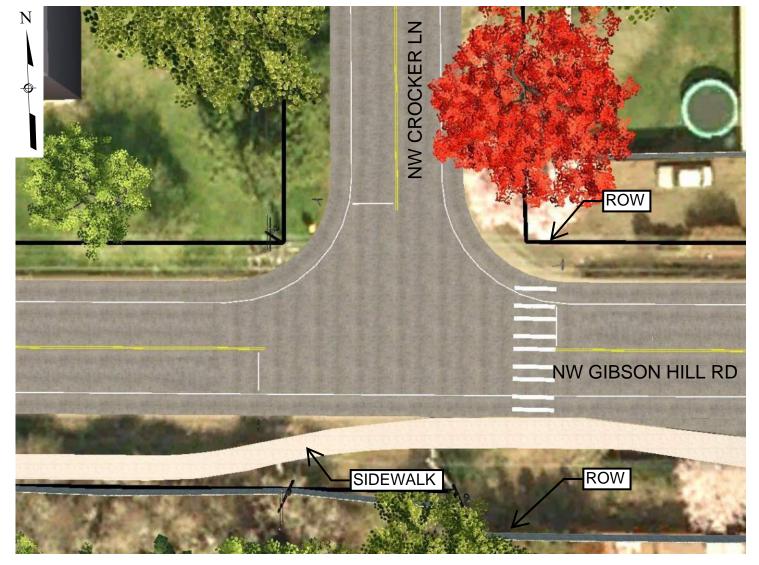


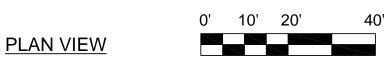


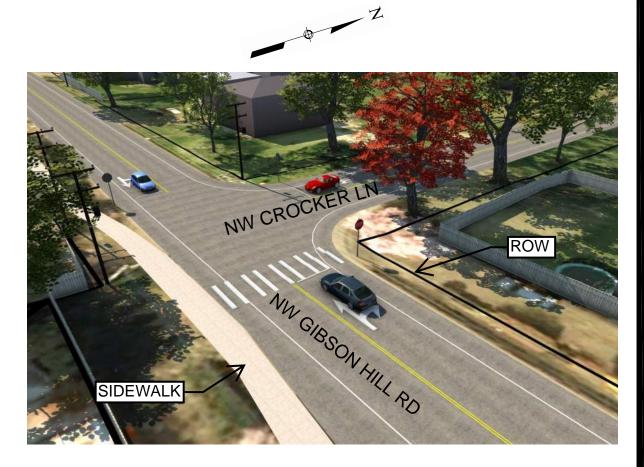




3. NO RIGHT-OF WAY IMPACTS







NW PERSPECTIVE VIEW

DATE:	1-27-16
DESIGN: DRAWN: CHECKED REVISION NUMBER:	

PROJECT NUMBER: ALBX00000044

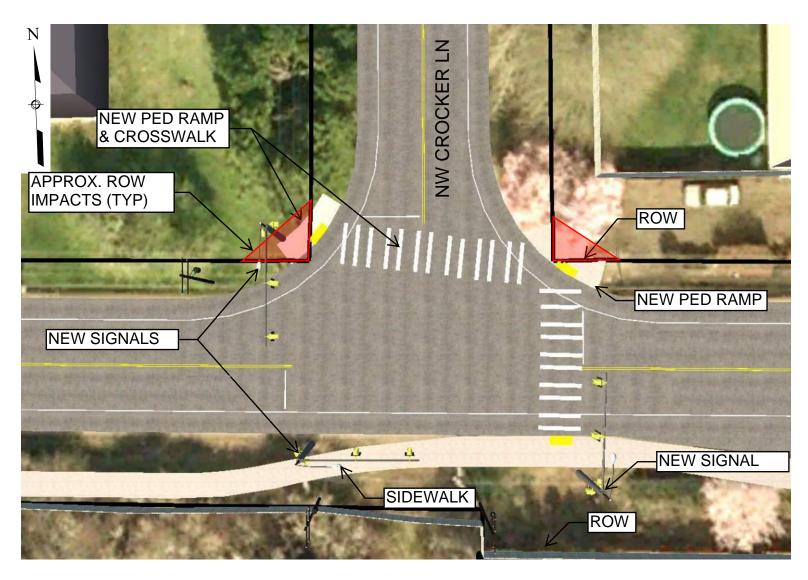
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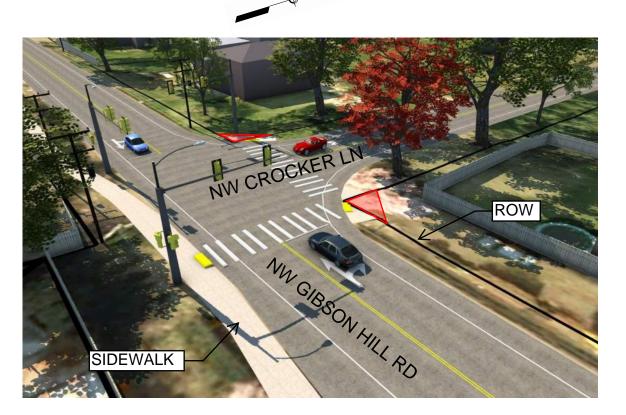
SHEET NO.

of 5

GENERAL NOTES:

- 1. INSTALL SIGNALS FOR EACH LEG
- 2. ADD PED RAMPS AT NE & NW CORNERS
- 3. REMOVE EXTG RECTANGULAR RAPID FLASHING BEACON
- 4. PAVEMENT WIDENING AT CURB RETURNS TO ACCOMMODATE WB-50 TURNS
- 5. MINIMAL ROW IMPACTS



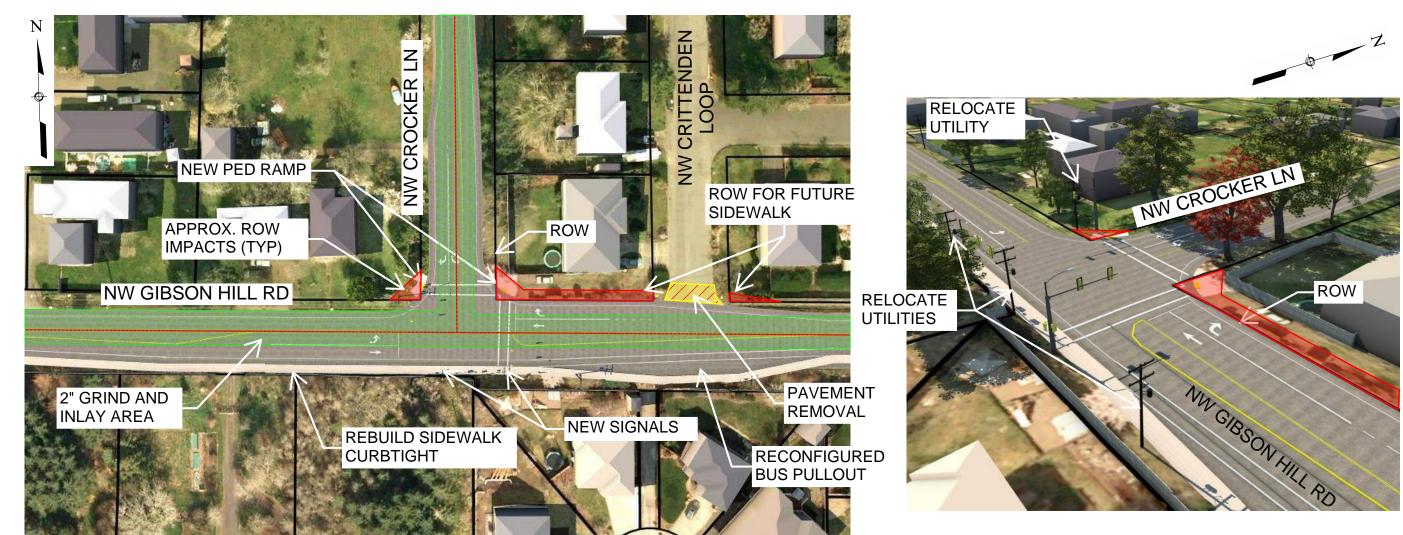


NW PERSPECTIVE VIEW

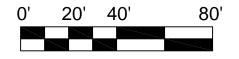
PLAN VIEW



- 1. INSTALL SIGNALS FOR EACH LEG
- 2. ADD PED RAMPS AT NE & NW CORNERS
- 3. REMOVE EXTG RECTANGULAR RAPID FLASHING BEACON
- 4. EASTBOUND GIBSON HILL LEFT TURN WIDENING TO SOUTH REBUILD SIDEWALK CURBTIGHT
- 5. WESTBOUND GIBSON HILL RIGHT TURN LANE WIDENED TO THE NORTH REQUIRES RESTRICTING ACCESS TO NW CRITTENDEN LOOP
- 6. ROW IMPACTS LOCALIZED TO THE NORTH
- 7. ASSUMED MINIMUM STORAGE LENGTHS & 25:1 ROADWAY SHIFT TAPERS
- 8. ROADWAY SECTION: 11' LANES, 12' TURN LANES, 5' SHOULDER/BIKE LANES, 6' SIDEWALK
- 9. BUS PULLOUT RECONFIGURED
- 10. ASSUME A SAWCUT & WIDEN WITH 2" GRIND & INLAY OF EXISTING PAVEMENT



PLAN VIEW



NW PERSPECTIVE VIEW

REVISION NUMBER:

PROJECT NUMBER: ALBX00000044

SHEET NO.

DATE: DESIGN: DRAWN: REVISION NUMBER:

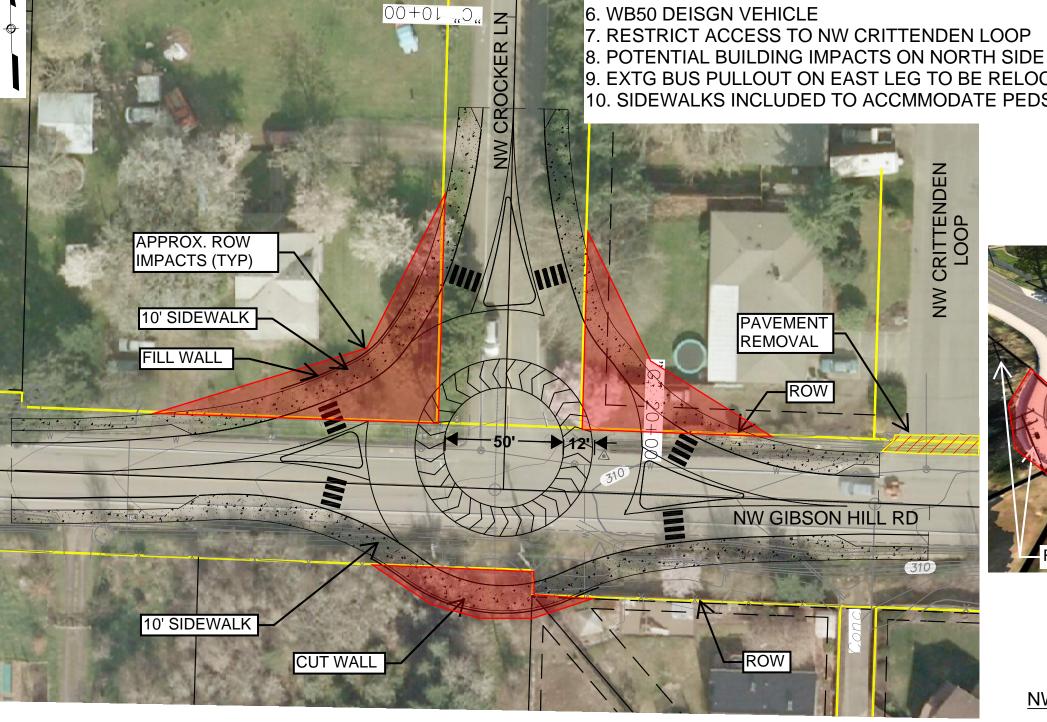
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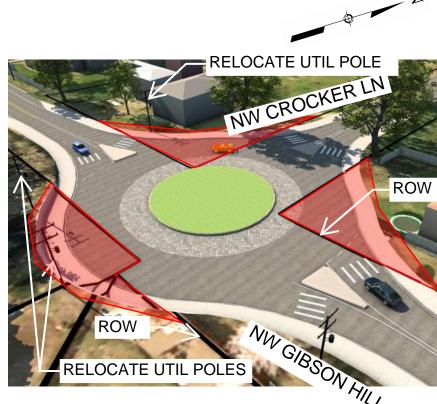
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GENERAL NOTES:

- 1. INSTALL 115' INSCRIBED DIAMETER CONCRETE ROUNDABOUT
- 2. 50' DIAMETER ISLAND W/12' TRUCK APRON
- 3. REMOVE EXTG RECTANGULAR RAPIC FLASHING BEACON
- 4. RIGHT-OF WAY IMPACTS TO NORTH & SOUTH SIDES COULD BE LOCALIZED TO ONE CORNER WITH A SIGNIFICANT SHIFT OF THE INTERSECTION
- 5. UTILITY RELOCATIONS REQUIRED

- 9. EXTG BUS PULLOUT ON EAST LEG TO BE RELOCATED (NOT INCLUDED IN PROJECT)
- 10. SIDEWALKS INCLUDED TO ACCMMODATE PEDS & BIKES THROUGH ROUNDABOUT





NW PERSPECTIVE VIEW

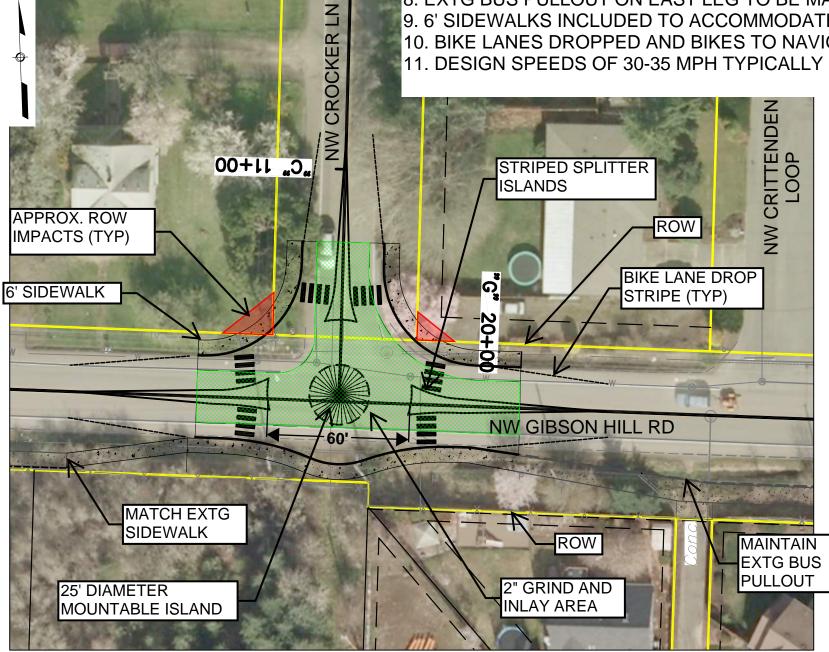
PLAN VIEW



SHEET NO.

GENERAL NOTES:

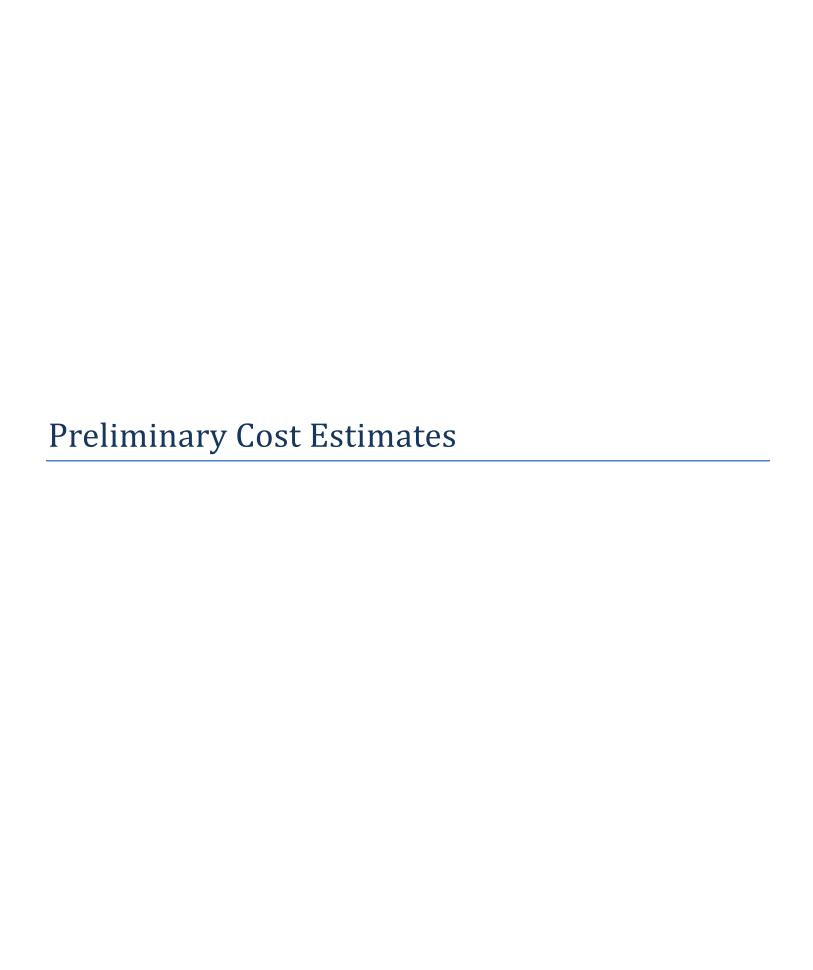
- 1. WIDEN FOR 60' INSCRIBED DIAMETER ASPHALT MINI-ROUNDABOUT
- 2. INSTALL 25' DIAMETER MOUNTABLE CENTER ISLAND
- 3. REMOVE EXTG RECTANGULAR RAPID FLASHING BEACON
- 4. STRIPED SPLITTER ISLANDS REQUIRED TO ACCOMMODATE WB-50 TURNING MOVEMENTS
- 5. RIGHT-OF WAY IMPACTS LOCALIZED TO NORTH
- 6. UTILITY RELOCATIONS REQUIRED
- 7. ASSUMED A SAWCUT & WIDEN WITH 2" GRIND & INLAY OF EXISTING PAVEMENT
- 8. EXTG BUS PULLOUT ON EAST LEG TO BE MAINTANED
- 9. 6' SIDEWALKS INCLUDED TO ACCOMMODATE PEDS
- 10. BIKE LANES DROPPED AND BIKES TO NAVIGATE ROUNDABOUT WITH VEHICLES
- 11. DESIGN SPEEDS OF 30-35 MPH TYPICALLY REQUIRED TO JUSTIFY MINI-ROUNDABOUT



NW GIBSON HILL RD RELOCATE UTIL POLES

PLAN VIEW

20' 40' 80'



	COST ESTIMATE OREGON STATE HIGHWAY DIV		•						
SECTION				CITY					
Gib	son Hill/Crocker Lane Intersection_Alt	1 All-Way S	top	Alba	Albany				
KEY NUMBER	кіnd of work Signing & Striping	LENGTH	DATE 2/16/16	ROADWAY DESIGNER David Evans	& Associates				
ITEM NUMBER	ITEM DESCRIPTION	UNIT	AMOUNT	UNIT COST	TOTAL				
_	N AND TRAFFIC CONTROL	- Citii	Amount	Citil CCC1	TOTAL				
	MOBILIZATION(10%)	LS	1	\$1,000	\$1,000				
	TRAFFIC CONTROL (10%)	LS	1	\$1,000	\$1,000				
ROADWAY	,	•		, ,	· ·				
PERMANENT	TRAFFIC CONTROL AND GUIDANCE DEVICES	•							
	SIGNS AND STRIPING	LS	1	\$3,000	\$3,000				
RIGHT OF WA	Y DEVELOPMENT								
SUBTOTAL, C	onstruction Items				\$5,000				
9800-0000150A	CONSTRUCTION ENGINEERING (15%)			\$1,000	\$1,000				
CONSTRUCTI	ON COST				\$6,000				
	CONTINGENCY		25%	\$1,500	\$1,500				
TOTAL CONS	TRUCTION COST				\$7,500				
PRELIMINARY	/ ENGINEERING COST		15%		\$2,000				
PROJECT GR	AND TOTALS				\$9,500				

SECTION				СІТҮ					
Gibson	Hill/Crocker Lane Intersection_Alt 2 Signa			Albany					
KEY NUMBER	KIND OF WORK	LENGTH	DATE 1/27/16	ROADWAY DESIGNER					
0	Paving, Signals, Signing, Striping	David Evans & Associates							
ITEM NUMBER		UNIT	AMOUNT	UNIT COST	TOTAL				
MOBILIZATIO	ON AND TRAFFIC CONTROL								
	MOBILIZATION(10%)	LS	1	\$23,000	\$23,000				
	TRAFFIC CONTROL (10%)	LS	1	\$23,000	\$23,000				
ROADWAY									
	REMOVAL OF STRUCTURES AND OBSTRUCTIONS	LS	1	\$4,000	\$4,000				
	GENERAL EXCAVATION / EMBANKMENT	CY	110	\$15	\$1,650				
	SUBGRADE GEOTEXTILE	SY	145	\$2	\$290				
	CONCRETE CURB & GUTTER	FOOT	140	\$20	\$2,800				
BASES									
	AGGREGATE BASE	TON	120	\$30	\$3,600				
WEARING SU	IRFACES								
	LEVEL 3, 1/2 INCH DENSE MHMAC MIXTURE	TON	60	\$100	\$6,000				
	CONCRETE SIDEWALK	SF	200	\$8	\$1,600				
PERMANENT	TRAFFIC CONTROL AND GUIDANCE DEVICES								
	SIGNS AND STRIPING	LS	1	\$3,000	\$3,000				
	SIGNAL	LS	1	\$200,000	\$200,000				
RIGHT OF WA	AY DEVELOPMENT								
	LANDSCAPE AND EROSION CONTROL (3%)	LS	1	\$1,000	\$1,000				
SUBTOTAL, O	Construction Items				\$270,000				
9800-0000150A	CONSTRUCTION ENGINEERING (15%)			\$41,000	\$41,000				
CONSTRUCT					\$311,000				
	CONTINGENCY		50%	\$156,000	\$156,000				
TOTAL CONS	TRUCTION COST				\$467,000				
DDEL IMPLACE	W ENGINEEDING COST		450/		A74.00				
PRELIMINAR	Y ENGINEERING COST	0.5	15%		\$71,00				
	PROPERTY IMPACTS	SF	260						
					.				
PROJECT GR	RAND TOTALS				\$538,00				

	COST ESTIMATE - 2 OREGON STATE HIGHWAY DIVISION		_						
SECTION				СІТУ					
Gibson	Hill/Crocker Lane Intersection_Alt 3 Signal	w/ Turr	Lanes	Albany					
KEY NUMBER	KIND OF WORK	LENGTH		ROADWAY DESIGNER					
0	Paving, Signals, Signing, Striping, Drainage		1/27/16	David Evans 8	& Associates				
ITEM NUMBER	ITEM DESCRIPTION	UNIT	AMOUNT	UNIT COST	TOTAL				
MOBILIZATIO	N AND TRAFFIC CONTROL								
	MOBILIZATION(10%)	LS	1	\$79,000	\$79,00				
	TRAFFIC CONTROL (10%)	LS	1	\$79,000	\$79,00				
ROADWAY									
	REMOVAL OF STRUCTURES AND OBSTRUCTIONS (5%)	LS	1	\$27,100	\$27,10				
	CLEARING AND GRUBBING	ACRE	1.0	\$5,000	\$5,00				
	GENERAL EXCAVATION / EMBANKMENT	CY	2100	\$15	\$31,500				
	SUBGRADE GEOTEXTILE	SY	2800	\$2	\$5,600				
	CONCRETE CURB & GUTTER	FOOT	2200	\$20	\$44,000				
DRAINAGE									
	DRAINAGE SYSTEM	FOOT	2200	\$80	\$176,000				
BASES									
	AGGREGATE BASE	TON	2200	\$30	\$66,000				
	2" COLD PLANE PAVEMENT REMOVAL	SY	3600	\$3	\$10,800				
WEARING SU									
	LEVEL 3, 1/2 INCH DENSE MHMAC MIXTURE	TON	1400	\$100	\$140,000				
	CONCRETE SIDEWALK	SF	5800	\$8	\$46,400				
PERMANENT	TRAFFIC CONTROL AND GUIDANCE DEVICES								
	SIGNS AND STRIPING	LS	1	\$15,000	\$15,000				
	SIGNAL	LS	1	\$200,000	\$200,000				
RIGHT OF WA	Y DEVELOPMENT			* 4 0 000	* 4.0.00				
	LANDSCAPE AND EROSION CONTROL (3%)	LS	1	\$16,000	\$16,000				
OUDTOTAL O					20.40.00				
	Construction Items			#110.000	\$942,000				
	CONSTRUCTION ENGINEERING (15%)			\$142,000	\$142,000				
CONSTRUCT			F00/	ΦE40.000	\$1,084,000				
TOTAL OCUO	CONTINGENCY		50%	\$542,000	\$542,00				
TOTAL CONS	TRUCTION COST				\$1,626,000				
DDEL MAINLA D	(FNOWEEDING COOT		450/		004100				
PKELIMINAR	Y ENGINEERING COST		15%		\$244,00				
	PROPERTY IMPACTS	SF	2100						
DDG IEGT CD	AND TOTAL O				A4 072 00				
PROJECT GR	AND TOTALS				\$1,870,000				

	COST ESTIMATE - 2 OREGON STATE HIGHWAY DIVISION		•		
SECTION				CITY	
	on Hill/Crocker Lane Intersection_Alt 4 Full	Rounda	hout	Alba	anv
KEY NUMBER	kind of work	LENGTH		ROADWAY DESIGNER	arry
0	Paving, Signing, Striping, Walls, Drainage	LENGIH	1/27/16	David Evans	& Associates
ITEM NUMBER	ITEM DESCRIPTION	UNIT	AMOUNT	UNIT COST	TOTAL
	N AND TRAFFIC CONTROL				75.7.1
	MOBILIZATION(10%)	LS	1	\$62,000	\$62,000
	TRAFFIC CONTROL (10%)	LS	1	\$62,000	\$62,000
ROADWAY	1.0.0.00			ψ02,000	Ψ02,000
	REMOVAL OF STRUCTURES AND OBSTRUCTIONS (5%)	LS	1	\$28,400	\$28,400
	CLEARING AND GRUBBING	ACRE	1.0	\$5,000	\$5,000
	GENERAL EXCAVATION / EMBANKMENT	CY	1300	\$15	\$19,500
	SUBGRADE GEOTEXTILE	SY	2700	\$2	\$5,400
	CONCRETE CURB & GUTTER	FOOT	1200	\$20	\$24,000
DRAINAGE	OCHORETE GORB & GOTTER	1001	1200	ΨΣΟ	Ψ24,000
DIVAINAGE	DRAINAGE SYSTEM	FOOT	1200	\$80	\$96,000
	DIVINACE CICIEM	1001	1200	φου	Ψ30,000
STRUCTURES					
STRUCTURES	lwalls	LS	1	\$40,000	\$40,000
	WALLO	- 10		Ψ+0,000	Ψ+0,000
BASES					
DAGES	AGGREGATE BASE	TON	2100	\$30	\$63,000
	AGGREGATE BASE	TON	2100	φου	\$63,000
WEARING SU	REACES				
WEARING OU	LEVEL 3, 1/2 INCH DENSE MHMAC MIXTURE	TON	300	\$100	\$30,000
	PLAIN CONCRETE PAVEMENT, 9" THICK	SY	1800	\$100	\$180,000
	CONCRETE SIDEWALK	SF	8600	\$8	\$68,800
	CONCRETE ISLANDS	SF	3200	\$8	\$25,600
			0200	40	+
PERMANENT	TRAFFIC CONTROL AND GUIDANCE DEVICES				
	SIGNS AND STRIPING	LS	1	\$10,000	\$10,000
				, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, ,,,,,,,,
RIGHT OF WA	Y DEVELOPMENT	'			
	LANDSCAPE AND EROSION CONTROL (3%)	LS	1	\$17,000	\$17,000
SUBTOTAL, C	Construction Items				\$737,000
9800-0000150A	CONSTRUCTION ENGINEERING (15%)			\$111,000	\$111,000
CONSTRUCTI	<u> </u>				\$848,000
	CONTINGENCY		50%	\$424,000	\$424,000
TOTAL CONS	TRUCTION COST				\$1,272,000
					, ,
PRELIMINARY	ENGINEERING COST		15%		\$191,000
	PROPERTY IMPACTS	SF	7300		
PROJECT GR	AND TOTALS				\$1,463,000

	COST ESTIMATE - 2 OREGON STATE HIGHWAY DIVISI							
SECTION				CITY				
Gibs	on Hill/Crocker Lane Intersection_Alt 5 Min	i Rounda	about	Alba	any			
KEY NUMBER	KIND OF WORK	LENGTH	DATE	ROADWAY DESIGNER				
0	Paving, Signing, Striping		2/16/16	David Evans	& Associates			
ITEM NUMBER	R ITEM DESCRIPTION	UNIT	AMOUNT	UNIT COST	TOTAL			
MOBILIZATIO	ON AND TRAFFIC CONTROL							
	MOBILIZATION(10%)	LS	1	\$12,000	\$12,000			
	TRAFFIC CONTROL (10%)	LS	1	\$12,000	\$12,000			
ROADWAY								
	REMOVAL OF STRUCTURES AND OBSTRUCTIONS (5%)	LS	1	\$5,400	\$5,400			
	CLEARING AND GRUBBING	ACRE	0.2	\$5,000	\$1,000			
	GENERAL EXCAVATION / EMBANKMENT	CY	400	\$15	\$6,000			
	SUBGRADE GEOTEXTILE	SY	350	\$2	\$700			
	CONCRETE CURB & GUTTER	FOOT	400	\$20	\$8,000			
DRAINAGE	·	•						
	DRAINAGE SYSTEM	FOOT	400	\$80	\$32,000			
STRUCTURE	S	•						
BASES			•					
	AGGREGATE BASE	TON	300	\$30	\$9,000			
	2" COLD PLANE PAVEMENT REMOVAL	SY	530	\$3	\$1,590			
WEARING SU	JRFACES							
	LEVEL 3, 1/2 INCH DENSE MHMAC MIXTURE	TON	200	\$100	\$20,000			
	CONCRETE SIDEWALK	SF	2300	\$8	\$18,400			
	CONCRETE ISLANDS	SF	490	\$8	\$3,920			
PERMANENT	TTRAFFIC CONTROL AND GUIDANCE DEVICES							
	SIGNS AND STRIPING	LS	1	\$6,000	\$6,000			
RIGHT OF W	AY DEVELOPMENT							
	LANDSCAPE AND EROSION CONTROL (3%)	LS	1	\$4,000	\$4,000			
	Construction Items				\$141,000			
9800-0000150A	CONSTRUCTION ENGINEERING (15%)			\$22,000	\$22,000			
CONSTRUCT					\$163,000			
	CONTINGENCY		50%	\$82,000	\$82,000			
TOTAL CONS	STRUCTION COST				\$245,000			
PRELIMINAR	RY ENGINEERING COST		15%		\$37,000			
	PROPERTY IMPACTS	SF	220					
PROJECT GF	RAND TOTALS				\$282,000			



Gibson Hill Road at Crocker Lane: 2040 Traffic Operations

	ΔM	Existing Configuration Alternative 1: All-Way Stop Alternative 1: All-Way Stop AM Peak Hour AM Peak Hour AM Peak Hour			ative :	·			Signal Hour		native	La	nes		th Turn		ernativ Peak	re 4: Mo		ounda I Peak		Alternative 5: Mini Roundabout AM Peak Hour PM Peak Hour														
																								Queue												
Overall													0.68	В		0.70	В		0.60			0.50														
EBL																			0.03		25	0.17		25												
EBLT	0.01	Α		0.07	Α	25	0.79	D	25	0.69	С	25.00	0.68	В	225	0.58	Α	175	0.63	В	200	0.48		125	0.73	В	250	0.51	Α				350	0.56	В	150
WBTR	0.01	Α		0.01	Α		0.49	С	25	1.10	F	25.00	0.39	Α	100	0.80	В	350	0.30	Α	75	0.57	Α	150	0.26	Α	50	0.70	В	250	0.27	Α	75	0.75	В	300
WBR																			0.05	Α	25	0.22	Α	25												
SBL																			0.56	В	150	0.36	В	100												
SBLR	1.00	F	25	0.87	F	25	0.74	С	25	0.35	В	25.00	0.67	В	200	0.46	В	125	0.08	Α	25	0.01	Α	25	0.49	В	100	0.28	Α	50	0.55	В	125	0.33	В	50
		-																																		

Int Delay, s/veh 27.									
iiii Delay, S/VeII 21.	.4								
Movement	EBL	EBT			WBT	WBR	SBL	SBR	
Traffic Vol, veh/h	15	445			200	70	305	110	
Future Vol, veh/h	15	445			200	70	305	110	
Conflicting Peds, #/hr	1	0			0	1	1	0	
Sign Control	Free	Free			Free	Free	Stop	Stop	
RT Channelized	-	None			-	None	-	None	
Storage Length	_	-			_	-	0	-	
Veh in Median Storage, #	_	0			0	_	0	_	
Grade, %	_	0			0	_	0	_	
Peak Hour Factor	95	95			95	95	95	95	
Heavy Vehicles, %	0	4			8	7	1	0	
Mvmt Flow	16	468			211	74	321	116	
		.00			_ ' '	- 11	- V21	- 110	
Maiau/Minau	Majard				\4-i0		Mins		
Major/Minor	Major1				Major2		Minor2	0.40	
Conflicting Flow All	285	0			-	0	748	249	
Stage 1	-	-			-	-	248	-	
Stage 2	-	-			-	-	500	-	
Critical Hdwy	4.1	-			-	-	6.41	6.2	
Critical Hdwy Stg 1	-	-			-	-	5.41	-	
Critical Hdwy Stg 2	-	-			-	-	5.41	-	
Follow-up Hdwy	2.2	-			-	-	3.509	3.3	
Pot Cap-1 Maneuver	1289	-			-	-	381	795	
Stage 1	-	-			-	-	796	-	
Stage 2	-	-			-	-	611	-	
Platoon blocked, %		-			-	-			
Mov Cap-1 Maneuver	1288	-			-	-	374	794	
Mov Cap-2 Maneuver	-	-			-	-	374	-	
Stage 1	-	-			-	-	795	-	
Stage 2	-	-			-	-	600	-	
Approach	EB				WB		SB		
HCM Control Delay, s	0.3				0		75.4		
HCM LOS	0.0						F		
							•		
Minor Long/Maior Minor	EDI	EDT	WDT	WDD CDL 4					
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR SBLn1					
Capacity (veh/h)	1288	-	-	- 435					
HCM Lane V/C Ratio	0.012	-	-	- 1.004					
HCM Control Delay (s)	7.8	0	-	- 75.4					
HCM Lane LOS	Α	Α	-	- F - 12.9					
HCM 95th %tile Q(veh)	0	-		- 12.9					

Intersection								
Int Delay, s/veh	10.8							
in Bolay, or voi:	10.0							
Mayamant	EBL	EBT			WBT	WBR	SBL	SBR
Movement Traffic Male value								
Traffic Vol, veh/h	55	350			425	290	150	20
Future Vol, veh/h	55	350			425	290	150	20
Conflicting Peds, #/hr	_ 1	0			0	1	1	0
Sign Control	Free	Free			Free	Free	Stop	Stop
RT Channelized	-	None			-	None	-	None
Storage Length	- -	-			-	-	0	-
Veh in Median Storage,		0			0	-	0	-
Grade, %	-	0			0	-	0	-
Peak Hour Factor	90	90			90	90	90	90
Heavy Vehicles, %	0	3			2	1	1	0
Mvmt Flow	61	389			472	322	167	22
Major/Minor	Major1				Major2		Minor2	
Conflicting Flow All	795	0			-	0	1145	635
Stage 1	-	_			-	-	634	_
Stage 2	-	_			_	-	511	-
Critical Hdwy	4.1	_			-	_	6.41	6.2
Critical Hdwy Stg 1	-	-			-	-	5.41	-
Critical Hdwy Stg 2	-	_			-	_	5.41	_
Follow-up Hdwy	2.2	-			-	-	3.509	3.3
Pot Cap-1 Maneuver	835	_			-	_	222	482
Stage 1	-	-			-	-	530	-
Stage 2	-	-			-	-	604	-
Platoon blocked, %		-			-	-		
Mov Cap-1 Maneuver	834	-			-	-	201	481
Mov Cap-2 Maneuver	-	-			-	-	201	-
Stage 1	-	-			-	-	530	-
Stage 2	-	-			-	-	547	-
Approach	EB				WB		SB	
HCM Control Delay, s	1.3				0		79.2 F	
HCM LOS							F	
Minor Lane/Major Mvmt		EBT	WBT	WBR SB				
Capacity (veh/h)	834	-	-		216			
HCM Lane V/C Ratio	0.073	-	-	- 0.				
HCM Control Delay (s)	9.7	0	-	- 7	79.2			
HCM Lane LOS	Α	Α	-	-	F			
HCM 95th %tile Q(veh)	0.2	-	-	-	6.9			

Intersection										
Intersection Delay, s/veh	23									
Intersection LOS	С									
Movement	EBU	EBL	EBT		WBU	WB ⁻	WBR	SBU	SBL	SBR
Traffic Vol, veh/h	0	15	445		0	200		0	305	110
Future Vol, veh/h	0	15	445		0	200		0	305	110
Peak Hour Factor	0.92	0.95	0.95		0.92	0.98		0.92	0.95	0.95
Heavy Vehicles, %	2	0	4		2	{		2	1	0
Mvmt Flow	0	16	468		0	21		0	321	116
Number of Lanes	0	0	1		0	•		0	1	0
Approach		EB				WE	3		SB	
Opposing Approach		WB				EF	3			
Opposing Lanes		1				•			0	
Conflicting Approach Left		SB							WB	
Conflicting Lanes Left		1				()		1	
Conflicting Approach Right						SE	3		EB	
Conflicting Lanes Right		0				•			1	
HCM Control Delay		26.8				15.1			24	
HCM LOS		D				()		С	
Lane	i i	EBLn1	WBLn1	SBLn1						
Vol Left, %		3%	0%	73%						
Vol Thru, %		97%	74%	0%						
Vol Right, %		0%	26%	27%						
Sign Control		Stop	Stop	Stop						
Traffic Vol by Lane		460	270	415						
LT Vol		15	0	305						
Through Vol		445	200	0						
RT Vol		0	70	110						
Lane Flow Rate		484	284	437						
Geometry Grp		1	1	1						
Degree of Util (X)		0.782	0.491	0.732						
Departure Headway (Hd)		5.817	6.219	6.035						
Convergence, Y/N		Yes	Yes	Yes						
Сар		615	583	594						
Service Time		3.913	4.219	4.129						
HCM Lane V/C Ratio		0.787	0.487	0.736						
HCM Control Delay		26.8	15.1	24						
HCM Lane LOS		D	С	С						
HCM 95th-tile Q		7.4	2.7	6.2						

Intersection										
Intersection Delay, s/veh	38.8									
Intersection LOS	Е									
Movement	EBU	EBL	EBT		WBU	WB ⁻	WBR	SBU	SBL	SBR
Traffic Vol, veh/h	0	55	350		0	425	5 290	0	150	20
Future Vol, veh/h	0	55	350		0	425		0	150	20
Peak Hour Factor	0.92	0.90	0.90		0.92	0.90	0.90	0.92	0.90	0.90
Heavy Vehicles, %	2	0	3		2	2	2 1	2	1	0
Mvmt Flow	0	61	389		0	472	322	0	167	22
Number of Lanes	0	0	1		0		0	0	1	0
Approach		EB				WE	3		SB	
Opposing Approach		WB				E	3			
Opposing Lanes		1				•			0	
Conflicting Approach Left		SB							WB	
Conflicting Lanes Left		1				()		1	
Conflicting Approach Right						SE	3		EB	
Conflicting Lanes Right		0				•			1	
HCM Control Delay		19.7				55.7	7		13.4	
HCM LOS		С				F	-		В	
Lane		EBLn1	WBLn1	SBLn1						
Vol Left, %		14%	0%	88%						
Vol Thru, %		86%	59%	0%						
Vol Right, %		0%	41%	12%						
Sign Control		Stop	Stop	Stop						
Traffic Vol by Lane		405	715	170						
LT Vol		55	0	150						
Through Vol		350	425	0						
RT Vol		0	290	20						
Lane Flow Rate		450	794	189						
Geometry Grp		1	1	1						
Degree of Util (X)		0.685	1	0.352						
Departure Headway (Hd)		5.481	5.055	6.705						
Convergence, Y/N		Yes	Yes	Yes						
Сар		657	723	536						
Service Time		3.536	3.055	4.742						
HCM Lane V/C Ratio		0.685	1.098	0.353						
HCM Control Delay		19.7	55.7	13.4						
HCM Lane LOS		С	F	В						
HCM 95th-tile Q		5.4	16.3	1.6						

	•	→	—	•	>	4		
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations		4	4		¥	02.11		
Traffic Volume (vph)	15	445	200	70	305	110		
Future Volume (vph)	15	445	200	70	305	110		
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750		
Total Lost time (s)	1100	4.0	4.0	1100	4.0	1100		
Lane Util. Factor		1.00	1.00		1.00			
Frpb, ped/bikes		1.00	0.99		1.00			
Flpb, ped/bikes		1.00	1.00		1.00			
Frt		1.00	0.96		0.96			
Flt Protected		1.00	1.00		0.96			
Satd. Flow (prot)		1682	1559		1616			
FIt Permitted		0.99	1.00		0.96			
Satd. Flow (perm)		1663	1559		1616			
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95		
· ·	16	468	211	74	321	116		
Adj. Flow (vph) RTOR Reduction (vph)	0		211	0	22	0		
\ \ ' '		0 484	263					
Lane Group Flow (vph)	0	404	∠03	0	415	0		
Confl. Peds. (#/hr)		40/	00/		1	00/		
Heavy Vehicles (%)	0%	4%	8%	7%	1%	0%		
Turn Type	Perm	NA	NA		Prot			
Protected Phases		2	6		4			
Permitted Phases	2							
Actuated Green, G (s)		18.0	18.0		16.0			
Effective Green, g (s)		18.0	18.0		16.0			
Actuated g/C Ratio		0.43	0.43		0.38			
Clearance Time (s)		4.0	4.0		4.0			
Vehicle Extension (s)		3.0	3.0		3.0			
Lane Grp Cap (vph)		712	668		615			
v/s Ratio Prot			0.17		c0.26			
v/s Ratio Perm		c0.29						
v/c Ratio		0.68	0.39		0.67			
Uniform Delay, d1		9.7	8.2		10.8			
Progression Factor		1.00	1.00		1.00			
Incremental Delay, d2		2.6	0.4		2.9			
Delay (s)		12.3	8.6		13.8			
Level of Service		В	Α		В			
Approach Delay (s)		12.3	8.6		13.8			
Approach LOS		В	А		В			
Intersection Summary								
HCM 2000 Control Delay			11.9	Н	CM 2000	Level of Service	В	
HCM 2000 Volume to Capac	city ratio		0.68			2.2.2.2.700		
Actuated Cycle Length (s)	,		42.0	Sı	um of lost	time (s)	8.0	
Intersection Capacity Utilizat	rion		70.9%		CU Level o		C	
Analysis Period (min)			15	10	. 5 2510. 0	. 5511166	<u> </u>	
A College Constant			10					

c Critical Lane Group

Queues

10: Gibson Hill Rd & Crocker Ln

1/22/2016

	→	←	\
Lane Group	EBT	WBT	SBL
Lane Group Flow (vph)	484	285	437
v/c Ratio	0.69	0.42	0.70
Control Delay	16.7	10.2	18.1
Queue Delay	0.0	0.0	0.0
Total Delay	16.7	10.2	18.1
Queue Length 50th (ft)	84	36	72
Queue Length 95th (ft)	212	102	202
Internal Link Dist (ft)	394	385	511
Turn Bay Length (ft)			
Base Capacity (vph)	1169	1108	1007
Starvation Cap Reductn	0	0	0
Spillback Cap Reductn	0	0	0
Storage Cap Reductn	0	0	0
Reduced v/c Ratio	0.41	0.26	0.43
Intersection Summary			

Gibson Hill Rd at Crocker Ln 1/5/2016 AM 2040 Signal - Single Lane Approaches David Evans and Associates, Inc.

Movement EBL EBT WBT WBR SBL SBR Lane Configurations ♣ ♣ ¥ ★ Traffic Volume (vph) 55 350 425 290 150 20	
Lane Configurations 4 1 1	
_ : : : : U : : : : :	
Hamic volume (volt) - 33 - 330 - 473 - 790 - 130 - 70	
Future Volume (vph) 55 350 425 290 150 20	
Ideal Flow (vphpl) 1750 1750 1750 1750 1750	
Total Lost time (s) 4.0 4.0 4.0	
Lane Util. Factor 1.00 1.00 1.00	
Frpb, ped/bikes 1.00 0.99 1.00	
Flpb, ped/bikes 1.00 1.00 1.00	
Frt 1.00 0.95 0.98	
Flt Protected 0.99 1.00 0.96	
Satd. Flow (prot) 1694 1614 1635	
Flt Permitted 0.79 1.00 0.96	
Satd. Flow (perm) 1340 1614 1635	
Peak-hour factor, PHF 0.90 0.90 0.90 0.90 0.90	
Adj. Flow (vph) 61 389 472 322 167 22	
RTOR Reduction (vph) 0 0 43 0 8 0	
Lane Group Flow (vph) 0 450 751 0 181 0	
Confl. Peds. (#/hr) 1 1 1	
Heavy Vehicles (%) 0% 3% 2% 1% 1% 0%	
Turn Type Perm NA NA Prot Protected Phases 2 6 8	
Permitted Phases 2	
, \ \ /	
, 3 ()	
•	
Clearance Time (s) 4.0 4.0	
Vehicle Extension (s) 3.0 3.0 3.0	
Lane Grp Cap (vph) 775 934 394	
v/s Ratio Prot c0.47 c0.11	
v/s Ratio Perm 0.34	
v/c Ratio 0.58 0.80 0.46	
Uniform Delay, d1 5.9 7.4 14.4	
Progression Factor 1.00 1.00 1.00	
Incremental Delay, d2 1.1 5.1 0.8	
Delay (s) 7.0 12.5 15.2	
Level of Service A B B	
Approach Delay (s) 7.0 12.5 15.2	
Approach LOS A B B	
Intersection Summary	
HCM 2000 Control Delay 11.1 HCM 2000 Level of Service B	
HCM 2000 Volume to Capacity ratio 0.70	
Actuated Cycle Length (s) 44.4 Sum of lost time (s) 8.0	
Intersection Capacity Utilization 87.2% ICU Level of Service E	
Analysis Period (min) 15	

c Critical Lane Group

	→	←	\
Lana Oracia	FDT	WDT	CDI
Lane Group	EBT	WBT	SBL
Lane Group Flow (vph)	450	794	189
v/c Ratio	0.59	0.83	0.48
Control Delay	10.1	16.1	20.6
Queue Delay	0.0	0.0	0.0
Total Delay	10.1	16.1	20.6
Queue Length 50th (ft)	59	112	40
Queue Length 95th (ft)	157	#352	104
Internal Link Dist (ft)	394	385	511
Turn Bay Length (ft)			
Base Capacity (vph)	1077	1316	640
Starvation Cap Reductn	0	0	0
Spillback Cap Reductn	0	0	0
Storage Cap Reductn	0	0	0
Reduced v/c Ratio	0.42	0.60	0.30
	J 2	J.53	- 0.00
Intersection Summary			

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

	٠	→	←	•	\	4			
ovement	EBL	EBT	WBT	WBR	SBL	SBR			
ne Configurations	*	†	†	7	*	7"			
fic Volume (vph)	15	445	200	70	305	110			
ire Volume (vph)	15	445	200	70	305	110			
Flow (vphpl)	1750	1750	1750	1750	1750	1750			
Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0			
e Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00			
, ped/bikes	1.00	1.00	1.00	0.98	1.00	1.00			
o, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00			
, position	1.00	1.00	1.00	0.85	1.00	0.85			
rotected	0.95	1.00	1.00	1.00	0.95	1.00			
I. Flow (prot)	1661	1683	1620	1361	1646	1488			
ermitted	0.63	1.00	1.00	1.00	0.95	1.00			
. Flow (perm)	1094	1683	1620	1361	1646	1488			
-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95			
Flow (vph)	16	468	211	74	321	116			
R Reduction (vph)	0	0	0	41	0	75			
Group Flow (vph)	16	468	211	33	321	41			
fl. Peds. (#/hr)	10	700	-11	1	1				
y Vehicles (%)	0%	4%	8%	7%	1%	0%			
Type	Perm	NA	NA	Perm	Prot	Perm			
cted Phases	1 Cilli	2	6	1 Cilli	4	1 Cilli			
nitted Phases	2		- U	6		4			
ated Green, G (s)	16.7	16.7	16.7	16.7	13.3	13.3			
tive Green, g (s)	16.7	16.7	16.7	16.7	13.3	13.3			
ated g/C Ratio	0.44	0.44	0.44	0.44	0.35	0.35			
ance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0			
cle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0			
e Grp Cap (vph)	480	739	711	598	576	520			
Ratio Prot	400	c0.28	0.13	330	c0.20	320			
Ratio Perm	0.01	60.20	0.13	0.02	60.20	0.03			
Ratio	0.01	0.63	0.30	0.02	0.56	0.03			
orm Delay, d1	6.1	8.3	6.9	6.1	10.0	8.3			
ression Factor	1.00	1.00	1.00	1.00	1.00	1.00			
emental Delay, d2	0.0	1.8	0.2	0.0	1.00	0.1			
ay (s)	6.1	10.1	7.1	6.2	11.1	8.3			
el of Service	Α	В	7.1 A	0.2 A	В	6.5 A			
roach Delay (s)	H	9.9	6.9	A	10.4	Λ			
roach LOS		9.9 A	0.9 A		10.4 B				
section Summary		, ,	, ,						
			0.4	1.1/	2000	Lovel of Comis		۸	
M 2000 Control Delay	oity rotio		9.4	П	JIVI 2000	Level of Service	3	Α	
1 2000 Volume to Capa	icity ratio		0.60	0.	ım of last	time (a)		0.0	
rated Cycle Length (s)	tion		38.0		um of lost			8.0	
ersection Capacity Utiliza	auon		50.4%	IC	U Level C	of Service		Α	
lysis Period (min) Critical Lane Group			15						
cai Lane Group									

	۶	→	←	•	\	4
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	ሻ	<u></u>	1	7	ሻ	7
Traffic Volume (veh/h)	15	445	200	70	305	110
Future Volume (veh/h)	15	445	200	70	305	110
Number	5	2	6	16	7	14
Initial Q (Qb), veh	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00			1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h/ln	1750	1683	1620	1636	1733	1750
Adj Flow Rate, veh/h	16	468	211	74	321	116
Adj No. of Lanes	1	1	1	1	1	1
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95
Percent Heavy Veh, %	0.95	0.93	0.95	7	0.95	0.95
•	611		704	604	470	424
Cap, veh/h		731				
Arrive On Green	0.43	0.43	0.43	0.43	0.28	0.28
Sat Flow, veh/h	1023	1683	1620	1389	1650	1487
Grp Volume(v), veh/h	16	468	211	74	321	116
Grp Sat Flow(s),veh/h/ln	1023	1683	1620	1389	1650	1487
Q Serve(g_s), s	0.3	6.2	2.4	0.9	4.9	1.7
Cycle Q Clear(g_c), s	2.7	6.2	2.4	0.9	4.9	1.7
Prop In Lane	1.00			1.00	1.00	1.00
Lane Grp Cap(c), veh/h	611	731	704	604	470	424
V/C Ratio(X)	0.03	0.64	0.30	0.12	0.68	0.27
Avail Cap(c_a), veh/h	1242	1770	1705	1461	1273	1148
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	6.1	6.3	5.2	4.8	9.1	7.9
Incr Delay (d2), s/veh	0.0	0.9	0.2	0.1	1.8	0.3
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.1	3.1	1.1	0.4	2.5	0.7
LnGrp Delay(d),s/veh	6.1	7.3	5.5	4.9	10.8	8.3
LnGrp LOS	Α	A	Α	A	В	Α
Approach Vol, veh/h		484	285		437	
Approach Delay, s/veh		7.2	5.3		10.1	
Approach LOS		Α	Α		В	
Timer	1	2	3	4	5	6
Assigned Phs		2		4		6
Phs Duration (G+Y+Rc), s		16.4		12.1		16.4
Change Period (Y+Rc), s		4.0		4.0		4.0
Max Green Setting (Gmax), s		30.0		22.0		30.0
Max Q Clear Time (g_c+I1), s		8.2		6.9		4.4
Green Ext Time (p_c), s		4.2		1.2		4.3
Intersection Summary						
HCM 2010 Ctrl Delay			7.8			
HCM 2010 LOS			Α			

	٠	→	←	•	>	4
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Group Flow (vph)	16	468	211	74	321	116
v/c Ratio	0.03	0.65	0.30	0.12	0.57	0.20
Control Delay	7.4	13.9	9.0	3.0	16.1	4.0
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	7.4	13.9	9.0	3.0	16.1	4.0
Queue Length 50th (ft)	2	65	24	0	48	0
Queue Length 95th (ft)	11	187	77	17	152	26
Internal Link Dist (ft)		394	385		511	
Turn Bay Length (ft)	150			150	150	
Base Capacity (vph)	879	1352	1302	1107	1024	970
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.02	0.35	0.16	0.07	0.31	0.12
Intersection Summary						

	٠	→	←	•	\	4		
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations	<u> </u>	<u></u>	1121	7	ሻ	T T		
Traffic Volume (vph)	55	350	425	290	150	20		
Future Volume (vph)	55	350	425	290	150	20		
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750		
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00		
Frpb, ped/bikes	1.00	1.00	1.00	0.98	1.00	1.00		
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00		
Frt	1.00	1.00	1.00	0.85	1.00	0.85		
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00		
Satd. Flow (prot)	1662	1699	1716	1442	1646	1488		
Flt Permitted	0.43	1.00	1.00	1.00	0.95	1.00		
Satd. Flow (perm)	746	1699	1716	1442	1646	1488		
Peak-hour factor, PHF	0.90	0.90	0.90	0.90	0.90	0.90		
Adj. Flow (vph)	61	389	472	322	167	22		
RTOR Reduction (vph)	0	0	0	167	0	16		
Lane Group Flow (vph)	61	389	472	155	167	6		
Confl. Peds. (#/hr)	1			1	1			
Heavy Vehicles (%)	0%	3%	2%	1%	1%	0%		
Turn Type	Perm	NA	NA	Perm	Prot	Perm		
Protected Phases		2	6		8			
Permitted Phases	2			6		8		
Actuated Green, G (s)	16.0	16.0	16.0	16.0	9.3	9.3		
Effective Green, g (s)	16.0	16.0	16.0	16.0	9.3	9.3		
Actuated g/C Ratio	0.48	0.48	0.48	0.48	0.28	0.28		
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0		
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0		
Lane Grp Cap (vph)	358	816	824	692	459	415		
v/s Ratio Prot		0.23	c0.28		c0.10			
v/s Ratio Perm	0.08			0.11		0.00		
v/c Ratio	0.17	0.48	0.57	0.22	0.36	0.01		
Uniform Delay, d1	4.9	5.8	6.2	5.0	9.6	8.7		
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00		
Incremental Delay, d2	0.2	0.4	1.0	0.2	0.5	0.0		
Delay (s)	5.1	6.3	7.2	5.2	10.1	8.7		
Level of Service	Α	Α	Α	Α	В	Α		
Approach Delay (s)		6.1	6.4		10.0			
Approach LOS		Α	Α		Α			
Intersection Summary								
HCM 2000 Control Delay			6.8	Н	CM 2000	Level of Service	е	
HCM 2000 Volume to Capa	acity ratio		0.50					
Actuated Cycle Length (s)			33.3	Sı	um of lost	time (s)		
Intersection Capacity Utiliza	ation		46.6%			of Service		
Analysis Period (min)			15					
- 0-11								

c Critical Lane Group

	•	→	←	•	\	4		
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations	7	<u></u>	1121	7	ኘ	7		
Traffic Volume (veh/h)	55	350	425	290	150	20		
Future Volume (veh/h)	55	350	425	290	150	20		
Number	5	2	6	16	3	18		
Initial Q (Qb), veh	0	0	0	0	0	0		
Ped-Bike Adj(A_pbT)	1.00	U	U	1.00	1.00	1.00		
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00		
Adj Sat Flow, veh/h/ln	1750	1699	1716	1733	1733	1750		
Adj Flow Rate, veh/h	61	389	472	322	167	22		
Adj No. of Lanes	1	1	1	1	107	1		
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90		
Percent Heavy Veh, %	0.50	3	2	1	1	0.50		
Cap, veh/h	490	939	948	813	288	260		
Arrive On Green	0.55	0.55	0.55	0.55	0.17	0.17		
Sat Flow, veh/h	639	1699	1716	1471	1650	1487		
Grp Volume(v), veh/h	61	389	472	322	167	22		
Grp Sat Flow(s), veh/h/ln	639	1699	1716	1471	1650	1487		
Q Serve(g_s), s	1.9	3.9	5.0	3.7	2.7	0.4		
Cycle Q Clear(g_c), s	6.9	3.9	5.0	3.7	2.7	0.4		
Prop In Lane	1.00	3.9	5.0	1.00	1.00	1.00		
	490	939	948	813	288	260		
Lane Grp Cap(c), veh/h	0.12	0.41	0.50	0.40	0.58	0.08		
V/C Ratio(X)	877	1968	1987	1704	1012	912		
Avail Cap(c_a), veh/h HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00		
	1.00	1.00	1.00	1.00	1.00	1.00		
Upstream Filter(I)	6.2		4.1	3.8	11.1			
Uniform Delay (d), s/veh		3.8	0.4		1.8	10.1		
Incr Delay (d2), s/veh	0.1	0.3	0.4	0.3		0.1		
Initial Q Delay(d3),s/veh	0.0	0.0		0.0	0.0			
%ile BackOfQ(50%),veh/ln	0.4	1.8	2.3	1.5	1.4	0.2		
LnGrp Delay(d),s/veh	6.3	4.1	4.5	4.1	13.0	10.3		
LnGrp LOS	A	A	A	A	B	В		
Approach Vol, veh/h		450	794		189			
Approach Delay, s/veh		4.4	4.3		12.6			
Approach LOS		Α	Α		В			
Timer	1	2	3	4	5	6	7	3
Assigned Phs		2				6		3
Phs Duration (G+Y+Rc), s		20.2				20.2	9.	
Change Period (Y+Rc), s		4.0				4.0	4.	
Max Green Setting (Gmax), s		34.0				34.0	18.	
Max Q Clear Time (g_c+l1), s		8.9				7.0	4.	
Green Ext Time (p_c), s		7.3				7.5	0.	
ntersection Summary								
HCM 2010 Ctrl Delay			5.4					
HCM 2010 Clif Delay			5.4 A					
IGIVI ZU IU LOG			А					

	•	→	←	•	\	1
Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Group Flow (vph)	61	389	472	322	167	22
v/c Ratio	0.17	0.49	0.58	0.38	0.37	0.05
Control Delay	6.5	8.4	9.8	2.3	14.5	6.7
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	6.5	8.4	9.8	2.3	14.5	6.7
Queue Length 50th (ft)	5	38	49	0	22	0
Queue Length 95th (ft)	22	104	133	25	80	12
Internal Link Dist (ft)		394	385		511	
Turn Bay Length (ft)	150			150	150	
Base Capacity (vph)	699	1591	1607	1370	940	860
Starvation Cap Reductn	0	0	0	0	0	0
Spillback Cap Reductn	0	0	0	0	0	0
Storage Cap Reductn	0	0	0	0	0	0
Reduced v/c Ratio	0.09	0.24	0.29	0.24	0.18	0.03
Intersection Summary						

Alternative 4 (2040)

MOVEMENT SUMMARY

₩ Site: 2040 AM

2040 Future Conditions Gibson Hill Road @ Crocker Lane - AM Peak Roundabout

Move	ment Perfo	rmance - Ve	hicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back o Vehicles veh	of Queue Distance ft	Prop. Queued	Effective Stop Rate per veh	Average Speed mph
East: 0	Gibson Hill R	d									
6	T1	247	8.0	0.256	5.0	LOSA	2.0	52.4	0.15	0.04	28.5
16	R2	86	7.0	0.256	4.9	LOS A	2.0	52.4	0.15	0.04	27.8
Appro	ach	333	7.7	0.256	5.0	LOS A	2.0	52.4	0.15	0.04	28.3
North:	Crocker Ln										
7	L2	321	1.0	0.488	10.3	LOS B	3.5	87.8	0.64	0.50	19.7
14	R2	116	0.0	0.488	10.2	LOS B	3.5	87.8	0.64	0.50	24.3
Appro	ach	437	0.7	0.488	10.2	LOS B	3.5	87.8	0.64	0.50	20.7
West:	Gibson Hill F	₹d									
5	L2	19	0.0	0.729	18.9	LOS B	9.3	239.1	0.91	0.90	19.6
2	T1	556	4.0	0.729	19.5	LOS B	9.3	239.1	0.91	0.90	24.7
Appro	ach	575	3.9	0.729	19.5	LOS B	9.3	239.1	0.91	0.90	24.5
All Vel	nicles	1345	3.8	0.729	12.9	LOS B	9.3	239.1	0.63	0.56	23.9

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project:

Alternative 4 (2040)

MOVEMENT SUMMARY

♥ Site: 2040 PM

2040 Future Conditions Gibson Hill Road @ Crocker Lane - AM Peak Roundabout

Move	ment Perfo	rmance - Ve	hicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back o Vehicles veh	of Queue Distance ft	Prop. Queued	Effective Stop Rate per veh	Average Speed mph
East: 0	Gibson Hill Ro	d									
6	T1	525	2.0	0.698	12.7	LOS B	9.2	234.1	0.54	0.26	26.0
16	R2	358	1.0	0.698	12.5	LOS B	9.2	234.1	0.54	0.26	25.4
Approa	ach	883	1.6	0.698	12.6	LOS B	9.2	234.1	0.54	0.26	25.7
North:	Crocker Ln										
7	L2	158	1.0	0.281	9.3	LOS A	1.7	43.1	0.73	0.66	19.8
14	R2	21	0.0	0.281	9.1	LOSA	1.7	43.1	0.73	0.66	24.4
Approa	ach	179	0.9	0.281	9.2	LOS A	1.7	43.1	0.73	0.66	20.2
West:	Gibson Hill R	ld									
5	L2	69	0.0	0.505	9.4	LOS A	4.3	110.6	0.59	0.39	21.3
2	T1	437	3.0	0.505	9.8	LOS A	4.3	110.6	0.59	0.39	27.5
Approa	ach	506	2.6	0.505	9.7	LOS A	4.3	110.6	0.59	0.39	26.4
All Veh	nicles	1568	1.8	0.698	11.3	LOS B	9.2	234.1	0.57	0.35	25.1

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Alternative 5 (2040)

MOVEMENT SUMMARY

♥ Site: 2040 AM

2040 Future Conditions Gibson Hill Road @ Crocker Lane - AM Peak Roundabout

Move	nent Perfo	rmance - Ve	hicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back o Vehicles veh	of Queue Distance ft	Prop. Queued	Effective Stop Rate per veh	Average Speed mph
East: 0	Bibson Hill Ro	d									
6	T1	247	8.0	0.274	5.5	LOSA	2.2	57.7	0.16	0.05	19.6
16	R2	86	7.0	0.274	5.4	LOS A	2.2	57.7	0.16	0.05	19.5
Approa	nch	333	7.7	0.274	5.5	LOS A	2.2	57.7	0.16	0.05	19.6
North:	Crocker Ln										
7	L2	321	1.0	0.553	12.8	LOS B	4.4	111.7	0.70	0.59	18.2
14	R2	116	0.0	0.553	12.7	LOS B	4.4	111.7	0.70	0.59	18.0
Approa	ach	437	0.7	0.553	12.8	LOS B	4.4	111.7	0.70	0.59	18.2
West:	Gibson Hill R	ld									
5	L2	19	0.0	0.833	29.2	LOS C	13.7	352.0	1.00	1.15	16.2
2	T1	556	4.0	0.833	29.9	LOS C	13.7	352.0	1.00	1.15	16.1
Approa	nch	575	3.9	0.833	29.8	LOS C	13.7	352.0	1.00	1.15	16.1
All Veh	icles	1345	3.8	0.833	18.3	LOS B	13.7	352.0	0.70	0.69	17.5

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Alternative 5 (2040)

MOVEMENT SUMMARY

₩ Site: 2040 PM

2040 Future Conditions Gibson Hill Road @ Crocker Lane - AM Peak Roundabout

Move	ment Perfo	rmance - Ve	hicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back o Vehicles veh	of Queue Distance ft	Prop. Queued	Effective Stop Rate per veh	Average Speed mph
East: 0	Sibson Hill Ro			••••••••••••••••••••••••••••••••••••••			VCII	- 10		per veri	Пірп
6	T1	525	2.0	0.754	15.6	LOS B	11.4	289.7	0.64	0.32	18.0
16	R2	358	1.0	0.754	15.5	LOS B	11.4	289.7	0.64	0.32	17.9
Approa	ach	883	1.6	0.754	15.6	LOS B	11.4	289.7	0.64	0.32	17.9
North:	Crocker Ln										
7	L2	158	1.0	0.333	11.7	LOS B	2.0	50.9	0.77	0.73	18.4
14	R2	21	0.0	0.333	11.5	LOS B	2.0	50.9	0.77	0.73	18.2
Approa	ach	179	0.9	0.333	11.6	LOS B	2.0	50.9	0.77	0.73	18.3
West:	Gibson Hill R	ld									
5	L2	69	0.0	0.561	11.4	LOS B	5.1	129.1	0.65	0.45	18.6
2	T1	437	3.0	0.561	11.8	LOS B	5.1	129.1	0.65	0.45	18.5
Approa	ach	506	2.6	0.561	11.7	LOS B	5.1	129.1	0.65	0.45	18.6
All Veh	icles	1568	1.8	0.754	13.9	LOS B	11.4	289.7	0.66	0.41	18.2

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Signalised Intersections.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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URBAN NON-SYSTEM CRASH LISTING

CITY OF ALBANY, BENTON COUNTY

GIBSON HILL RD and CROCKER LN, City of Albany, Benton County, 01/01/2010 to 12/31/2014

Total crash records: 6

	S D	7.7									anai iian									
	P R S		CT A CC	OTTY OTDERT	DD GUAD	INT-TYPE		OFFRD	MULID	CD A CII	SPCL USE	MOME			A 5	,				
SER#	EAUC		CLASS	CITY STREET FIRST STREET	RD CHAR DIRECT	(MEDIAN) LEGS	INT-REL		WTHR SURF	CRASH COLL	TRLR QTY OWNER	MOVE FROM	חשמת	INJ			חבט			
	E L G H D C S L		DIST FROM	SECOND STREET	LOCTN	(#LANES)	TRAF- CONTL	RNDBT	LIGHT	SVRTY	V# TYPE	TO	PRTC P# TYPE			E LICNS		ERROR	ACT EVENT	CAUSE
00129	N N N	02/19/2010		CROCKER LN	INTER	3-LEG	N	N	CLR	ANGL-OTH	01 NONE 0	TURN-L	1 1111	DVICE		<u> </u>	100	Бинон	TICI BVBIVI	03
NONE		FR	0	GIBSON HILL RD	CN		STOP SIGN	N	DRY	TURN	PRVTE	N -E							000	00
		7P			01	0		N	DLIT	PDO	PSNGR CAR		01 DRVR	NONE	00 F	OR-Y		020	000	03
																OR<25				
											02 NONE 0	STRGHT							000	00
											PRVTE PSNGR CAR	W -E	01 DRVR	NONE	23 F	OR-Y		000	000	00
											ronon onn		01 211111	1,01,2	23 1	OR<25				
80189	N N N N	N 02/25/2010	16	CROCKER LN	INTER	3-LEG	N	N	CLD	ANGL-OTH	01 NONE 0	STRGHT							079	02
CITY		TH	0	GIBSON HILL RD	CN		STOP SIGN	N	DRY	TURN	PRVTE	E -W							000	00
		4P			01	0		N	DAY	INJ	PSNGR CAR		01 DRVR	INJC	26 M			000	000	00
											00 NONE 0	minni i				OR<25				
											02 NONE 0 PRVTE	TURN-L N -E							000	00
											PSNGR CAR	1, 1	01 DRVR	NONE	17 F	OR-Y		028	000	02
																OR<25				
00448	N N N N	N 06/25/2010	16	CROCKER LN	INTER	3-LEG	N	N	CLR	BIKE										02
CITY		FR	0	GIBSON HILL RD	CN		STOP SIGN	N	DRY	TURN		-								
		5P			01	0		N	DAY	INJ		STRGHT	01 BIKE	INJA	64 F		I XWK?	000	000	00
											01 NONE 0	E W TURN-L								
											PRVTE	N -E							000	00
											PSNGR CAR		01 DRVR	NONE	17 M	OR-Y		027	000	02
																OR<25				
00837	N N N	12/03/2013	16	CROCKER LN	INTER	3-LEG	N	N	CLR	ANGL-OTH	01 NONE 0	STRGHT								02
NONE		TU	0	GIBSON HILL RD	CN		STOP SIGN	N	DRY	TURN	PRVTE	E -W							000	00
		7A			01	0		N	DAWN	INJ	PSNGR CAR		01 DRVR	INJC	61 F			000	000	00
											02 NONE 0	TURN-L				OR<25				
											PRVTE	N -E							015	00
											PSNGR CAR		01 DRVR	NONE	18 M	OR-Y		028	000	02
																OR<25				
00033	N N N	01/13/2010		GIBSON HILL RD	STRGHT		N	N	FOG	ANIMAL	01 NONE 0	STRGHT							035	12
NONE		WE	30	CROCKER LN	E	(NONE)	UNKNOWN	N	DRY	OTH	PRVTE	W -E							000 035	00
		7A			05	(02)		N	DAWN	PDO	PSNGR CAR		01 DRVR	NONE	44 F	OR-Y OR<25		000	000	12
00085	NI NI NI NI	N 02/04/2011	16	GIBSON HILL RD	STRGHT	(02)	N	N	CLR	S-1STOP	01 NONE 0	STRGHT				01(~23				27,07
CITY	TA TA TA TA	FR	20	CROCKER LN	SIRGHI W	(NONE)	NONE	N N	DRY	S-ISTOP REAR	PRVTE	SIRGHI W -E							000	00
		7A	•		06	, /	-	N	DAY	INJ	PSNGR CAR	=	01 DRVR	NONE	18 F	OR-Y		043	000	07
						(02)										OR<25				
											02 NONE 0	STOP								
											PRVTE	W -E	מזממ 1.0	TNITO	21 □	OB 37		000	011 000	00
											PSNGR CAR		01 DRVR	TNOC	34 F	OR-Y OR<25		000	000	00
																01(~2)				

URBAN NON-SYSTEM CRASH LISTING

CITY OF ALBANY, BENTON COUNTY

GIBSON HILL RD and Intersectional Crashes at GIBSON HILL RD, City of Albany, Benton County, 01/01/2010 to 12/31/2014

Total crash records: 29

	S D	м									apar nan									
	P R S					INT-TYPE					SPCL USE									
	EAUC		CLASS	CITY STREET	RD CHAR		INT-REL	OFFRD	WTHR	CRASH	TRLR QTY	MOVE			A :					
R#	ELGH	R DAY	DIST	FIRST STREET	DIRECT	LEGS	TRAF-	RNDBT	SURF	COLL	OWNER	FROM	PRTC	INJ	G I	E LICNS	PED			
/EST	D C S L	K TIME	FROM	SECOND STREET	LOCTN	(#LANES)	CONTL	DRVWY	LIGHT	SVRTY	V# TYPE	TO	P# TYPE	SVRTY	E 2	X RES	LOC ER	ROR	ACT EVENT	CAUSE
31	N N N	06/30/2013		N ALBANY RD	INTER	CROSS	N	N	CLR	S-1STOP	01 NONE 0	STRGHT								07
ΙE		SU	0	GIBSON HILL RD	W		YIELD	Y	DRY	REAR	PRVTE	W -E							000	00
		7A			06	0		N	DAY	PDO	PSNGR CAR		01 DRVR	NONE	39 F	OR-Y OR<25	02	6	000	07
											02 NONE 0	STOP								
											PRVTE	M -E							011	00
											PSNGR CAR		01 DRVR	NONE	00 M	UNK UNK	0.0	0	000	00
00	N N N N	N 12/26/2013	16	N ALBANY RD	INTER	CROSS	N	N	FOG	S-1STOP	01 NONE 0	STRGHT								07
ГҮ		TH	0	GIBSON HILL RD	W		YIELD	Y	DRY	REAR	PRVTE	N -S							000	00
		5P			06	0		N	DUSK	INJ	PSNGR CAR		01 DRVR	NONE	33 F	OR-Y	02	6	000	07
											02 NONE 0	STOP				OR<25				
											PRVTE	N -S							011	00
											PSNGR CAR	~	01 DRVR	INJC:	37 F	OR-Y	00	0	000	00
																OR<25				
	N N N N	N 11/02/2013		N ALBANY RD	INTER	CROSS	N	N	UNK	S-1STOP	01 NONE 0	STRGHT							092	02
NE		SA	0	GIBSON HILL RD	CN		YIELD	N	UNK	REAR	PRVTE	UN-UN							000	00
		9A			04	0		N	DAY	PDO	PSNGR CAR		01 DRVR	NONE	35 M	OR-Y OR<25	02	6	000	07
											02 NONE 0	STOP								
											PRVTE	UN-UN							011	26
											PSNGR CAR		01 DRVR	NONE	30 M	OR-Y OR<25	00	0	000	00
190	N N N	03/30/2014	16	N ALBANY RD	INTER	CROSS	N	N	CLR	ANGL-OTH	01 NONE 0	TURN-R								12
NE		SU	0	GIBSON HILL RD	CN		YIELD	Y	DRY	TURN	PRVTE	W -S							000	00
		8A			03	0		N	DAY	PDO	PSNGR CAR		01 DRVR	NONE	88 F	OR-Y OR<25	00	0	026	12
											02 NONE 0	STRGHT								
											PRVTE	N -S							000	00
											PSNGR CAR		01 DRVR	NONE	19 M	OR-Y OR<25	00	0	000	00
817	N N N N	N 11/20/2014	16	N ALBANY RD	INTER	CROSS	N	Y	RAIN	FIX OBJ	01 NONE 0	STRGHT							050	27
TY			0	GIBSON HILL RD	CN		YIELD	Y	WET	FIX	PRVTE	W -E							000 050	00
		11P			03	0		N	DLIT	INJ	PSNGR CAR		01 DRVR	INJC	45 M	OR-Y OR<25	01	6,081	038	27
414	N N N	06/11/2011	16	GIBSON HILL RD	STRGHT		N	N	CLR	ANIMAL	01 NONE 0	STRGHT							035	00
RPT		SA	100	N ALBANY RD	W	(NONE)	NONE	N	DRY	OTH	PRVTE	W -E							000 035	00
=		10P			08	/		N	DARK	PDO	PSNGR CAR		01 DRVR	NONE	16 M	OR-Y	00	0	000	00
						(02)										OR<25				
375	N N N	11/30/2010	16	THORN DR	INTER	3-LEG	N	N	RAIN	S-1STOP	01 NONE 0	STRGHT				-				07
Y.	TA TA TA		0	GIBSON HILL RD	E	2 DEG	UNKNOWN	N	WET	S-ISTOP REAR	PRVTE	E -W							000	00
- 1		6P	U	GIDSON HILL KD	<u>н</u> 06	0	OTMICINOWIN	N	DUSK	INJ	PSNGR CAR	M	01 DRVR	TMTC	16 M	OR-Y	04	3	000	07
		OT.				J		TA	DODIC	1110	02 NONE 0	STOP	OT DIVER	11V0 C	10 M	OR-1 OR<25	04	-	300	0 1
											02 NONE 0 PRVTE	E -W							012	00
											PRVTE PSNGR CAR	ъ -W	01 DRVR	TMTC	20 M	OR-Y	00	n	000	00
													OI DAVA	TINUC	∠ <i>∋</i> №	OR-1 OR<25				
557	N N N N	N 08/21/2014		GIBSON HILL RD	ALLEY		N	N	CLR	BIKE	01 NONE 0	TURN-R								02
TY		TH	85	PARK TER	E	(NONE)	NONE	N	DRY	TURN	PRVTE	S -E							018	00

Disclaimer: The information contained in this report is compiled from individual driver and police crash reports submitted to the Oregon Department of Transportation as required in ORS 811.720. The Crash Analysis and Reporting Unit is committed to providing the highest quality crash data to customers. However, because submittal of crash report forms is the responsibility of the individual driver, the Crash Analysis and Reporting Unit can not guarantee that all qualifying crashes are represented nor can assurances be made that all details pertaining to a single crash are accurate. Note: Legislative changes to DMV's vehicle crash reporting requirement, effective 01/01/2004, may result in fewer property damage only crashes being eligible for inclusion in the Statewide Crash Data File.

URBAN NON-SYSTEM CRASH LISTING

CITY OF ALBANY, BENTON COUNTY

GIBSON HILL RD and Intersectional Crashes at GIBSON HILL RD, City of Albany, Benton County, 01/01/2010 to 12/31/2014

Total crash records: 29

	S D P R S W				INT-TYPE					SPCL USE									
	E A U C O DATE	CLASS	CITY STREET	RD CHAR	(MEDIAN)	INT-REL	OFFRD	WTHR	CRASH	TRLR QTY	MOVE			Α	S				
ER#	E L G H R DAY	DIST	FIRST STREET	DIRECT	LEGS	TRAF-	RNDBT	SURF	COLL	OWNER	FROM	PRTC	INJ	G	E LICN	S PED			
NVEST	D C S L K TIME	FROM	SECOND STREET	LOCTN	(#LANES)	CONTL	DRVWY		SVRTY	V# TYPE	TO	P# TYPE	SVRTY		X RES	LOC	ERROR	ACT EVENT	CAUSE
	7₽			07	(02)		N	DAY	INJ	PSNGR CAR		01 DRVR	NONE	73 I	OR-Y		027	000	02
											STRGHT E W	01 BIKE	INJB	19 N	1	ВКРАТН	000	047	18
1923	Y N N N N 12/13/2010	17	NORTH HEIGHTS DR	INTER	3-LEG	N	N	RAIN	S-1STOP	01 NONE 0	STRGHT								07,01
TY	MO	0	GIBSON HILL RD	E		UNKNOWN	N	WET	REAR	PRVTE	E -W							000	00
	5P			06	0		N	DARK	PDO	PSNGR CAR		01 DRVR	NONE	32 N	OR-Y		043,047	000	07,01
										02 NONE 0	STOP								
										PRVTE	E -W	0.4						011	00
										PSNGR CAR		01 DRVR	NONE	38 1	OR-Y		000	000	00
134	N N N 02/28/2013	16	BROADWAY ST	INTER	3-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT							013	07
NE	TH	0	GIBSON HILL RD	W		UNKNOWN	N	DRY	REAR	PRVTE	M -E							000	00
	1P			06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	INJC	26 I	OR-Y		026	000	07
										02 NONE 0	STOP							011 012	0.0
										PRVTE PSNGR CAR	W -E	01 DRVR	NONE	68 I	M OR-Y		000	011 013 000	00
										03 NONE 0	STOP				Oleva	5			
										PRVTE	W -E							022	00
										PSNGR CAR		01 DRVR	NONE	56 I	F OR-Y UNK		000	000	00
146	N N N N N 03/03/2013	16	BROADWAY ST	INTER	CROSS	N	N	CLR	S-1STOP	01 NONE 0	STRGHT								32,27
TY	SU	0	GIBSON HILL RD	W		UNKNOWN	N	DRY	REAR	PRVTE	W -E							000	00
	6P			06	0		N	DARK	INJ	PSNGR CAR		01 DRVR	NONE	66 I	OR-Y		052,016,026	000	32,27
										02 NONE 0	STOP								
										PRVTE	W -E							012	00
										PSNGR CAR		01 DRVR	INJC	25 N	OR-Y		000	000	00
129	N N N 02/19/2010	16	CROCKER LN	INTER	3-LEG	N	N	CLR	ANGL-OTH	01 NONE 0	TURN-L								03
NE	FR	0	GIBSON HILL RD	CN		STOP SIGN	N	DRY	TURN	PRVTE	N -E							000	00
	7 _P			01	0		N	DLIT	PDO	PSNGR CAR		01 DRVR	NONE	00 I	OR-Y		020	000	03
										02 NONE 0	STRGHT								
										PRVTE	W -E	01 55	NT	00 -	. 05		000	000	00
										PSNGR CAR		01 DRVR	NONE	23 I	OR-Y		000	000	0.0
	N N N N N 02/25/2010			INTER	3-LEG	N	N	CLD	ANGL-OTH		STRGHT							079	02
TY		0	GIBSON HILL RD	CN		STOP SIGN	N	DRY	TURN	PRVTE	E -W							000	00
	4P			01	0		N	DAY	INJ	PSNGR CAR		01 DRVR	INJC	26 N	OR-Y		000	000	00
										02 NONE 0	TURN-L							200	0.0
										PRVTE PSNGR CAR	N -E	01 DRVR	NONE	17 I	OR-Y		028	000	00 02
)448	N N N N N 06/25/2010	16	CROCKER LN	INTER	3-LEG	N	N	CLR	BIKE				-		0.11.12	-			02

URBAN NON-SYSTEM CRASH LISTING

CITY OF ALBANY, BENTON COUNTY

GIBSON HILL RD and Intersectional Crashes at GIBSON HILL RD, City of Albany, Benton County, 01/01/2010 to 12/31/2014

Total crash records: 29

	S D																				
	P R S	W					INT-TYPE					SPCL USE									
	E A U C	O DATE	CLASS	(CITY STREET	RD CHAR	(MEDIAN)	INT-REL	OFFRD	WTHR	CRASH	TRLR QTY	MOVE			A	S				
ER#	E L G H	R DAY	DIST	1	FIRST STREET	DIRECT	LEGS	TRAF-	RNDBT	SURF	COLL	OWNER	FROM	PRTC	INJ	G	E LICNS	PED			
NVEST ITY	D C S L	K TIME FR	FROM 0		SECOND STREET GIBSON HILL RD	LOCTN CN	(#LANES)	CONTL STOP SIGN	DRVWY N	LIGHT DRY	SVRTY TURN	V# TYPE	<u>TO</u>	P# TYPE	SVRTY	E	X RES	LOC	ERROR	ACT EVENT	CAUSE
		5P	Ü	·	012001 11122 112	01	0	5101 5101	N	DAY	INJ		STRGHT	01 BIKE	INJA	64	F	I XWK?	000	000	00
													E W								
												01 NONE 0	TURN-L							0.00	0.0
												PRVTE PSNGR CAR	N -E	01 DRVR	NONE	17 1	M OR-Y		027	000	00 02
												I BNOK CAR		OI DRVR	NONE	Ι, ,	OR<25		027	000	02
0837	N N N	12/03/2013	1	.6 (CROCKER LN	INTER	3-LEG	N	N	CLR	ANGL-OTH	01 NONE 0	STRGHT								02
ONE		TU	0	(GIBSON HILL RD	CN		STOP SIGN	N	DRY	TURN	PRVTE	E -W							000	00
		7A				01	0		N	DAWN	INJ	PSNGR CAR		01 DRVR	INJC	61			000	000	00
												02 NONE 0	TURN-L				OR<25				
												PRVTE	N -E							015	00
												PSNGR CAR		01 DRVR	NONE	18	M OR-Y		028	000	02
																	OR<25				
0033	N N N	01/13/2010	1	.7 (GIBSON HILL RD	STRGHT		N	N	FOG	ANIMAL	01 NONE 0	STRGHT							035	12
IONE		WE	30	(CROCKER LN	E	(NONE)	UNKNOWN	N	DRY	OTH	PRVTE	W -E							000 035	00
		7A				05	(02)		N	DAWN	PDO	PSNGR CAR		01 DRVR	NONE	44	F OR-Y OR<25		000	000	12
0085	N N N N	N 02/04/2011	1	.6 (GIBSON HILL RD	STRGHT	(02)	N	N	CLR	S-1STOP	01 NONE 0	STRGHT				01(123				27,07
ITY	10 10 10 10	FR	20		CROCKER LN	W	(NONE)	NONE	N	DRY	REAR	PRVTE	W -E							000	00
		7A	20	·		06	(110112)	110112	N	DAY	INJ	PSNGR CAR		01 DRVR	NONE	18	F OR-Y		043	000	07
							(02)										OR<25				
												02 NONE 0	STOP								
												PRVTE	W -E							011	00
												PSNGR CAR		01 DRVR	INJC	34	F OR-Y OR<25		000	000	00
<u>0513</u>	N N N N	N 05/19/2014	1	.6 (CRITTENDON LP	INTER	3-LEG	N	N	UNK	ANGL-OTH	01 NONE 0	STRGHT				010 123				02
O RPT	14 14 14 14	MO	0		GIBSON HILL RD	CN	3 1110	STOP SIGN	N	UNK	TURN	PRVTE	UN-UN							000	00
		4A				03	0		N	DARK	PDO	PSNGR CAR		01 DRVR	NONE	78	M OR-Y		000	000	00
																	OR<25				
												02 NONE 0	UNK								
												PRVTE	UN-UN							015	00
												PSNGR CAR		01 DRVR	NONE	22 1	M OR-Y OR<25		028	000	02
0583	NNNN	N 08/01/2012	1	.6 (GIBSON HILL RD	INTER	3-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT								32,27
ITY	1, 1, 1, 1,	WE	0		GRANDVIEW DR	W	3 110	UNKNOWN	N	DRY	REAR	PRVTE	W -E							000	00
		5P				06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	NONE	17	M OR-Y		052,016,026	000	32,27
																	OR<25				
												02 NONE 0	STOP								
												PRVTE	M -E	01					000	012	00
												PSNGR CAR		01 DRVR	INJC	32	F OR-Y OR<25		000	000	00
)295	N N N	05/14/2014	1	.6 (GIBSON HILL RD	GRADE		N	N	CLR	S-1STOP	01 NONE 0	STRGHT				310.133				12
ONE		WE	30		GIBSON HILL WAY	E	(NONE)	UNKNOWN	N	DRY	REAR	PRVTE	W -E							000	00
		6P				05	,		N	DAY	INJ	PSNGR CAR		01 DRVR	NONE	22	F OR-Y		026	026	12
							(02)										OR>25				
												02 NONE 0	STOP								
												PRVTE PSNGR CAR	W -E	01 DRVR					000	011 000	0 0 0 0

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URBAN NON-SYSTEM CRASH LISTING

CITY OF ALBANY, BENTON COUNTY

GIBSON HILL RD and Intersectional Crashes at GIBSON HILL RD, City of Albany, Benton County, 01/01/2010 to 12/31/2014

Page: 4

Total crash records: 29

	S D																	
	P R S W				INT-TYPE					SPCL USE								
	E A U C O DATE	CLASS	CITY STREET	RD CHAR		INT-REL	OFFRD		CRASH	TRLR QTY	MOVE			A :				
SER#	E L G H R DAY	DIST	FIRST STREET	DIRECT	LEGS	TRAF-	RNDBT		COLL	OWNER	FROM		INJ		E LICNS PED			
INVEST	D C S L K TIME	FROM	SECOND STREET	LOCTN	(#LANES)	CONTL	DRVWY	LIGHT	SVRTY	V# TYPE 02 NONE 0	TO STOP	P# TYPE	SVRTY	E .	X RES LOC	ERROR	ACT EVENT	CAUSE
										PRVTE	W -E						011	00
										PSNGR CAR		02 PSNG	INJB	02 F		000	000	00
										02 NONE 0 PRVTE	STOP W -E						011	00
										PSNGR CAR	,, _	03 PSNG	NO<5	01 F		000	000	00
00232	N N N 04/03/2010	16	GIBSON HILL RD	INTER	3-LEG	N	N	RAIN	S-1STOP	01 NONE 0	STRGHT							07
CITY	SA	0	PULVER LN	E		UNKNOWN	N	WET	REAR	PRVTE	E -W						000	00
	2P			06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	NONE	18 M		026	000	07
										02 NONE 0	STOP				OR<25			
										PRVTE	E -W						012	00
										PSNGR CAR		01 DRVR	INJB	16 F	UNK	000	000	00
															OR<25			
										02 NONE 0	STOP						010	0.0
										PRVTE PSNGR CAR	E -W	02 PSNG	TNJC	12 ೯		012 000	0 0 0 0	
										I BIVOIC CAIC		02 1510	11100	12 1		000	000	00
0099	N N N N N 01/29/2010	16	GIBSON HILL RD	INTER	3-LEG	N	N	CLR	O-1TURN	01 NONE 0	TURN-L						079	02
CITY	FR	0	PULVER LN	CN		NONE	N	DRY	TURN	PRVTE	E -S						000	00
	12P			03	0		N	DAY	INJ	PSNGR CAR		01 DRVR	INJB	16 M		004	000	02
										0.2 MONTE 0	CMD CLIM				OR<25			
										02 NONE 0 PRVTE	STRGHT W -E						000 079	00
										PSNGR CAR	,, _	01 DRVR	NONE	34 F	OR-Y	000	000	00
															OR<25			
80153	N N N N N 02/05/2014	4 16	GIBSON HILL RD	INTER	3-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT						002	07,27
CITY	WE	0	PENNY LN	E		UNKNOWN	N	DRY	REAR	PRVTE	E -W						000	00
	1P			06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	NONE	34 F	OR-Y OR<25	043,026	038 002	07,27
										01 NONE 0	STRGHT				UR<25			
										PRVTE	E -W						000	00
										PSNGR CAR		02 PSNG	NO<5	02 F		000	000	00
										01 NONE 0 PRVTE	STRGHT E -W						000	00
										PSNGR CAR	E -W	03 PSNG	NO<5	04 M		000	000	00
												12 10110	0 .0					
										02 NONE 0	STOP							
										PRVTE	E -W	0.5					011	00
										PSNGR CAR		01 DRVR	INJC	68 F	OR-Y OR<25	000	000	00
10380	N N N N N 06/16/2014	4 16	GIBSON HILL RD	STRGHT		Y	N	CLR	S-STRGHT	01 NONE 0	STRGHT				OK-23		093	27,07
CITY	MO MO	36	PENNY LN	SIRGHI W	(NONE)	stop sign	N	DRY	S-SIRGHI REAR	PRVTE	W -E						000	00
	6P	*		06	,	. 3-4-	N	DAY	INJ	PSNGR CAR	•	01 DRVR	NONE	41 M	OR-Y	016,042	038 093	27,07
					(02)										OR<25			
										02 NONE 0	STRGHT							0.5
										PRVTE PSNGR CAR	W -E	01 DRVR	TM.TC	57 M	OR-V	000	000 000	0 0 0 0
										FONGK CAR		UI DKVK	TINUC	الاا / د	0K-1	000	000	00

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URBAN NON-SYSTEM CRASH LISTING

CITY OF ALBANY, BENTON COUNTY

GIBSON HILL RD and Intersectional Crashes at GIBSON HILL RD, City of Albany, Benton County, 01/01/2010 to 12/31/2014

Total crash records: 29

	S D																				
	P R S	W				INT-TYPE					SPCL USE										
	E A U C	O DATE	CLASS	CITY STREET	RD CHAR	(MEDIAN)	INT-REL	OFFRD	WTHR	CRASH	TRLR QTY	MOVE				A S					
ER#	E L G H	R DAY	DIST	FIRST STREET	DIRECT	LEGS	TRAF-	RNDBT	SURF	COLL	OWNER	FROM	PRTC	INJ		G E	LICNS	PED			
NVEST	D C S L	K TIME	FROM	SECOND STREET	LOCTN	(#LANES)	CONTL	DRVWY	LIGHT	SVRTY	V# TYPE	то	P# TYPE	SVR	TY	E X	RES OR<25	LOC	ERROR	ACT EVENT	CAUSE
0451	N N N	06/04/2012	16	GIBSON HILL RD	GRADE		Y	N	RAIN	S-1STOP	01 NONE 0	STRGHT									07
NONE		MO	20	PENNY LN	E	(NONE)	UNKNOWN	N	WET	REAR	PRVTE	E -W								022	00
		4 P			06	(02)		N	DAY	PDO	PSNGR CAR		01 DRVR	NON	E 1	5 M	OR-Y OR<25		026	000	07
											02 NONE 0	STOP									
											PRVTE	E -W								011	00
											PSNGR CAR		01 DRVR	NON	E 6	4 F	OR-Y OR<25		000	000	00
											03 NONE 0	STRGHT									
											PRVTE	E -W								000	00
											PSNGR CAR		01 DRVR	NON	E 4	3 F	OR-Y OR<25		000	000	00
00580 N N N NONE	N N N	08/27/2011	16	GIBSON HILL RD	INTER	3-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT									07
		SA	0	SKYLINE DR	E		UNKNOWN	N	DRY	REAR	PRVTE	E -W								000	00
		10A			06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	NON	E 1	3 F	OR-Y OR<25		026	000	07
											02 NONE 0	STOP									
											PRVTE	E -W								012	00
											PSNGR CAR		01 DRVR	INJ	C 1	7 M	OR-Y OR<25		000	000	00
323	N N N N	N 05/22/2014	16	GIBSON HILL RD	INTER	3-LEG	N	N	CLR	S-1STOP	01 NONE 0	STRGHT									07
ITY		TH	0	SKYLINE DR	E		STOP SIGN	N	DRY	REAR	PRVTE	E -W								000	00
		2P			06	0		N	DAY	INJ	PSNGR CAR		01 DRVR	INJ	C 6:	2 F	OR-Y		043,026	000	07
											02 NONE 0	STOP					OR<25		·		
											PRVTE	E -W								012	00
											PSNGR CAR		01 DRVR	INJ	C 1	9 F	OR-Y OR<25		000	000	00
764	N N N	11/07/2014	16	GIBSON HILL RD	INTER	3-LEG	N	N	CLR	ANGL-OTH	01 NONE 0	STRGHT									02
1E		FR	0	SKYLINE DR	CN		STOP SIGN	N	DRY	TURN	PRVTE	W -E								000	00
		7P			04	0		N	DLIT	INJ	PSNGR CAR		01 DRVR	INJ	В 3	7 M	OR-Y OR<25		000	000	00
											02 NONE 0	TURN-L									
											PRVTE	S -W								000	00
											PSNGR CAR		01 DRVR	NON	E 1'	7 F	OR-Y OR<25		028	000	02
17	N N N	01/09/2014	16	GIBSON HILL RD	STRGHT		N	N	RAIN	S-1STOP	01 NONE 0	STRGHT									29
NONE		TH	150	SKYLINE DR	W	(NONE)	UNKNOWN	N	WET	REAR	PRVTE	W - E								000	00
		7A			08	(02)		N	DLIT	PDO	PSNGR CAR		01 DRVR	NON	E 2	M C	OR-Y OR<25		026	000	29
											02 NONE 0	STOP									
											PRVTE	W -E								011	00
											PSNGR CAR		01 DRVR	NON	E 5	7 M	OR-Y		000	000	00
																	OR<25				